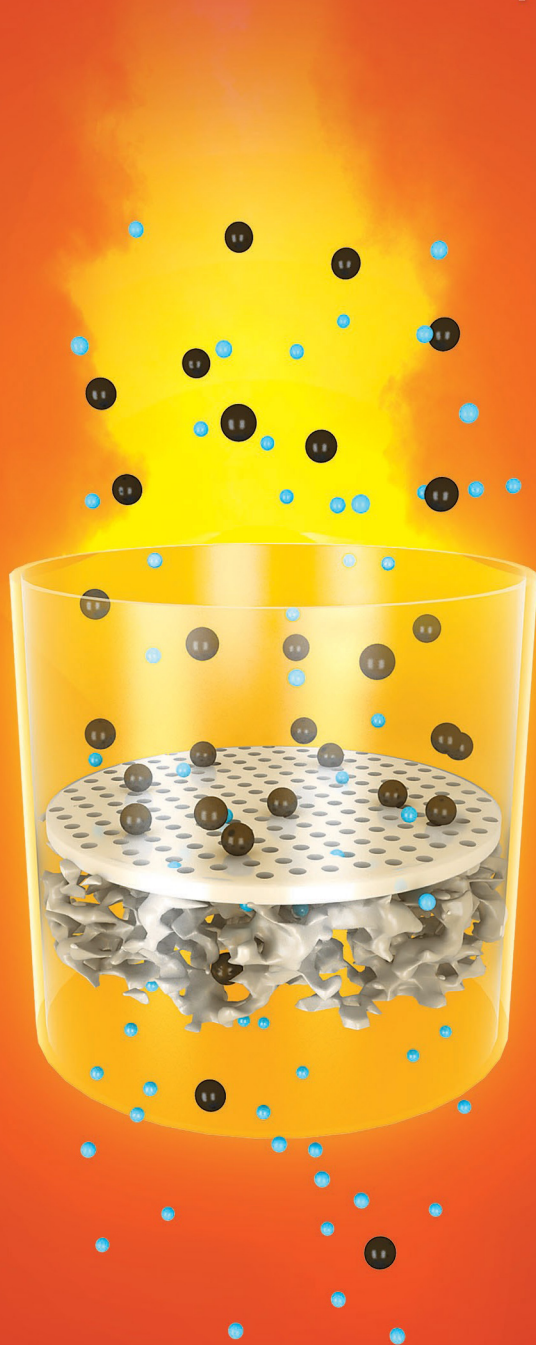


# Orchestrating Pore Structure of Hybrid Silica Membranes for Molecular Separations



Hammad Fayyaz Qureshi

**ORCHESTRATING PORE STRUCTURE  
OF HYBRID SILICA MEMBRANES FOR  
MOLECULAR SEPARATIONS**

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# **ORCHESTRATING PORE STRUCTURE OF HYBRID SILICA MEMBRANES FOR MOLECULAR SEPARATIONS**

DISSERTATION

to obtain  
the degree of doctor at the University of Twente,  
on the authority of the rector magnificus,  
Prof. dr. H. Brinksma,  
on account of the decision of the graduation committee,  
to be publicly defended  
on Thursday, the 26<sup>th</sup> of June 2014 at 16:45

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*Humans are also membranes; only selective people permeate through our compatibility barriers and get access to our minds and hearts*



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# **Chapter 1**

## **Introduction**

## 1.1 General Introduction

A membrane is a permselective barrier between two phases. It facilitates a faster transport of a specific component compared to others present in the feed, which results in a purified or a separated stream. Membrane-based separations are considered a preferred separation method due to their uncomplicated operation in process development schemes aiming at decreasing the production costs, energy utilization and waste generation [1].

In general, membranes are classified as either organic (polymeric) or inorganic membranes, according to the materials they are made of. For molecular separation, the polymeric membranes commonly in use for gas separation are made of cellulose acetate, polysulfone, polyamide, polyimide, etc. They commonly show relatively good permeability, but their performance is majorly hindered by poor thermal and chemical stability [2]. By comparison with conventional polymeric membranes, inorganic membranes offer an improvement in thermal and chemical stability, which is a substantial advantage. Inorganic membranes have been developed by using various materials such as silica, alumina, titania, or zirconia that resulted in membranes with a porous microstructure [2-4].

According to IUPAC definitions, porous membranes can be categorized into macroporous (pore diameter  $> 50$  nm), mesoporous ( $50 >$  pore diameter  $> 2$  nm) and microporous (pore diameter  $< 2$ nm) membranes [5]. Based on the pore size, separation processes ranging from microfiltration to gas separation can be exploited by using porous inorganic membranes.

Porous inorganic membranes can either be symmetric or asymmetric in their structure. Symmetric membranes have a single layer of a porous inorganic material possessing a considerable thickness for mechanical stability [4]. However to obtain large fluxes the separation layer thickness must be as small as possible. Thin separation layers can be achieved by using an asymmetric configuration where a selective top layer is mounted on a porous support thus forming a graded structure. The support is generally made from a metal oxide on top of which layers are applied with gradually decreasing pore size.

This thesis focuses on asymmetric microporous membranes for gas separation. The stacked system of interest in this work is an  $\alpha$ -alumina (macroporous) /  $\gamma$ -alumina or hybrid silica (mesoporous) / hybrid silica (microporous) membrane. The macroporous support has a thickness of about 2 mm (pore size:  $d_p$  50-70 nm) that provides essential mechanical strength to the stack. On top of this support, an intermediate mesoporous layer is coated, having a thickness of 3  $\mu\text{m}$  (pore size:  $d_p$  4-5 nm). The main purpose of such an intermediate layer is to provide sufficient smoothness and sufficient small pore size for the deposition of a very thin gas selective layer. This microporous top layer has a thickness of few tens to few hundred nanometers and is responsible for the gas separation properties of the membrane. Amongst porous inorganic membranes, silica membranes are a prime candidate for gas separation due to their small pore size ( $d_p < 0.5$  nm), the relative easy way of fabrication, low production costs and scalability [4, 6].

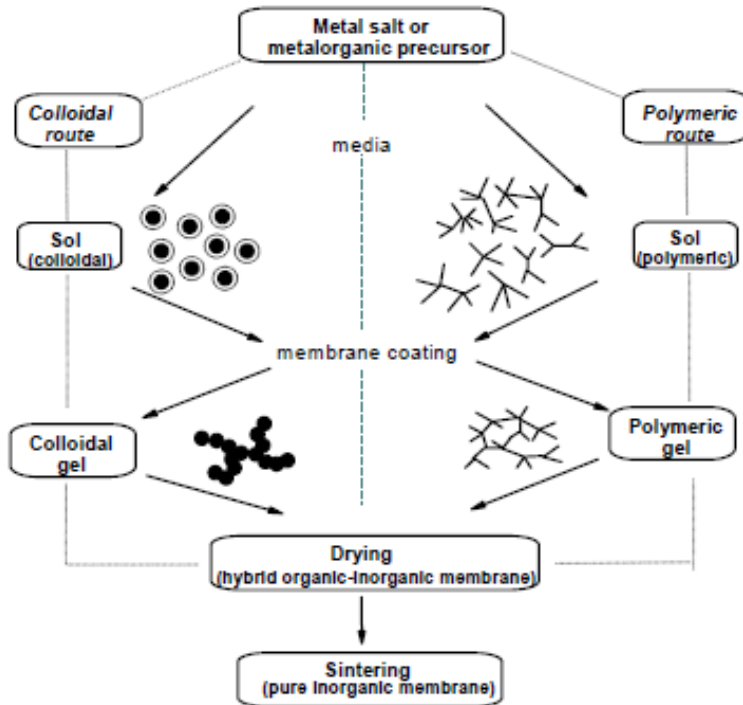
### **1.2 Sol-gel derived microporous silica membranes: Synthesis and structural properties**

Sol-gel processing is a wet chemical technique that offers a wide variety in reaction tunability and choice of precursors for the fabrication of microporous ceramic membranes. The fabrication of microporous silica membranes by means of the sol-gel technique has been a focus in research for the past few decades [7-9].

Sol-gel processing offers two routes to develop an inorganic membrane *i.e.* either via a colloidal or a polymeric sol. In the colloidal route, the synthesis takes place in an aqueous medium while in polymeric route it occurs in an alcoholic medium. In the colloidal route the colloids remain isolated due to electrostatic repulsion, whereas in the polymeric route the sol particles remain separated in solution because of their small size. In both cases the condensation reactions occur at the sol stage with the formation of colloids or clusters which later on interact to form a gel. Both routes yield nano-sized particles from which porous materials can be developed. The polymeric route yields particles useful for making microporous materials and membranes [10].

Inorganic membrane fabrication by sol-gel processing is usually done by dip-coating with subsequent thermal treatment (sintering/calcining) in the temperature range

between 400 and 800 °C. Figure 1.1 summarizes the fabrication procedure of inorganic membranes by sol-gel processing.



**Figure 1.1:** Sol-gel routes commonly used to make inorganic membranes [10].

Microporous silica membranes are made by sol-gel processing following the polymeric route. Silica sols, typically synthesized in acid environments, are deposited on porous substrates in a dust-free environment. The resulting supported layer undergoes a thermal treatment of at least 400 °C which results in a microporous membrane having a pore size of approximately 0.4 nm and a thickness of a few tens of nanometers [9, 11, 12]. They show good separation properties for various gas mixtures, such as  $H_2/CO_2$ ,  $H_2/N_2$ ,  $H_2/CH_4$ , and in some cases these membranes were found nitrogen and methane impermeable [13, 14]. However, these membranes were found unstable in water vapor, particularly at high temperatures; that is, the gas permeance decreases with time under hydrothermal conditions, resulting in a decreased overall gas permselectivity. This membrane

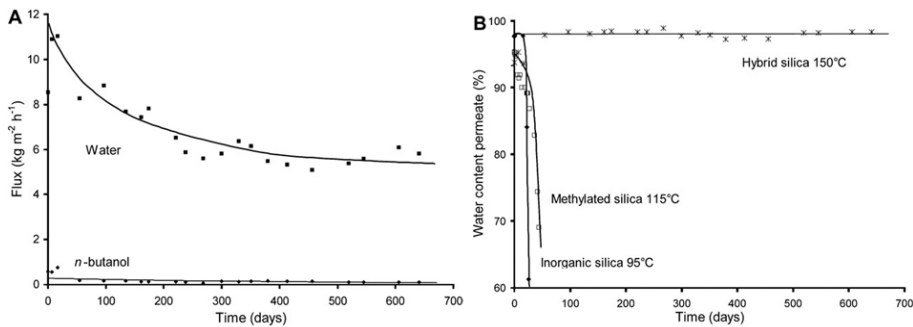
instability is due to the continuous condensation of the silanol groups in the amorphous silica structure, which is accelerated at high temperatures under humid conditions. This results in the densification of the silica matrix starting with closing of the small pores leading to the formation of larger pores and eventually ends up in a complete delamination of the selective top layer [3, 15, 16].

This limitation with silica membranes could be overcome by using an organic–inorganic hybrid silica, which contains at least one organic group that cannot be hydrolyzed, such as methyltriethoxysilane (MTES), to control the pore size under hydrothermal conditions [17-20]. In these references, hybrid organic–inorganic polymeric sols and membranes were prepared by the copolymerization of TEOS and MTES. However, these modifications did not sufficiently increase the hydrothermal stability of membranes and the membrane structure deteriorated within 100 days under pervaporation conditions (shown in figure 1.2) [21]. Another attempt to improve the hydrothermal stability of silica membranes is to incorporate metal ions such as Zr, Al, Ni, Nb and Co to the silica matrix [22-26]. For Co [27, 28] and Nb [29, 30] doping a considerable improvement in the performance of silica membranes under hydrothermal conditions was found. However, for Zr, Al, Mg, and Ni-doped silica, no improvement in hydrothermal stability was found [24, 31, 32].

### 1.3 Hybrid silica Membranes for Molecular Separation

Castricum et al. [21, 33-36] developed organosilica membranes starting from bridged *bis*(silyl) precursors: *bis*(triethoxysilyl)ethane (BTESE) and *bis*(triethoxysilyl)methane (BTESEM), with methyltriethoxysilane (MTES) showing superior hydrothermal stability if compared with silica-derived membranes. These type of membranes will now be termed as hybrid silica membranes in this chapter. The BTESE/MTES membranes showed high solvolytical and long-term acid stability for almost 2 years during the dehydration of *n*-butanol at 150 °C, as shown in figure 1.2. The authors proposed that the enhanced durability of these hybrid silica membranes, if compared with pure silica membranes, was due to the incorporation of organic linking groups [21]. As the organic groups are nonpolar, they “shield” the siloxane bonds from water, which leads to less concomitant hydrolysis [37] that is pivotal in maintaining the consistency in performance of BTESE membranes for an extended period of time.





**Figure 1.2:** Long-term separation performance of BTESE/MTES hybrid silica membranes for dehydration of *n*-butanol (5 wt. % water) by pervaporation at 150 °C. **(A)** A 4% change in H<sub>2</sub>O-flux was observed in 700 days. **(B)** Very high water selectivity was observed by these membranes at 150 °C in comparison with inorganic and methylated silica membranes [21].

The viability of BTESE membranes in gas separation was first exploited by Tsuru et. al [38, 39]. They developed a BTESE membrane that showed a H<sub>2</sub>-permeance in the range of 10<sup>-5</sup> mol/[m<sup>2</sup>.s.Pa] at 200 °C with a H<sub>2</sub>/N<sub>2</sub> permselectivity of less than 10. The reported synthesis was a very complicated multi-step sol synthesis. The formation of the hybrid sols in this case was discontinuous as the reaction was stopped and water was added at various times during the synthesis. This procedure resulted in an irregular pore microstructure and formed less selective membranes. Therefore, a systematic engineering of pores on structural level must be pursued to exploit the application window of this material with tailor-made pore sizes for targeting small molecular separations.

## 1.4 Aim of the thesis

The main focus of this thesis is the development of molecular sieving hybrid silica (BTESE) membranes by sol-gel processing, with substantial improvement and precision in their pore size and pore-size distribution to render them suitable for gas separation applications. This stresses an in-depth understanding of the sol-gel process parameters and their implications in forming a defect-free selective film that would result in molecular separation performance equal (or close) to conventional silica membranes.

A systematic investigation, targeting hybrid silica (BTESE) sols and gels, will be carried out to examine the influence of sol-gel process conditions and doping of metal ions into the hybrid silica materials on the pore size and performance of BTESE membranes. Sol process parameters such as reaction time and temperature, acid catalyst, hydrolysis ration and dip-sol rheology will be studied in detail and their implication in making a defect-free microporous layer will be examined. The realization of incorporating a metal ion in a hybrid silica network is not a straightforward route due to the mismatch in reactivities between the precursors. The fabrication recipe must be tuned and optimized with the aid of varying either process conditions or the reactivity of precursors. In addition to that, the prospects of fabricating a mesoporous hybrid-silica intermediate layer as a substitute of gamma-alumina will be studied.

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## **Chapter 2**

# **Influence of sol-gel process parameters on the micro-structure and performance of hybrid silica membranes**

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## Abstract

A facile, versatile and reproducible sol-gel process to make microporous organosilica membranes by using 1,2-*bis* (triethoxysilyl) ethane (BTESE) as a precursor is reported. The influence of process parameters on sol particle size and rheology of BTESE-derived sols was investigated to produce defect-free composite membranes by a single dipping procedure and subsequent calcination. The microporous structure of a BTESE layer on mesoporous alumina supports enabled selective molecular sieving of gas molecules. Single gas permeation (SGP) experiments, performed at 200°C, showed that a H<sub>2</sub>/CH<sub>4</sub> permselectivity of 24 was reproducibly achieved. No SF<sub>6</sub> gas permeance through these membranes proof the presence of a defect-free microstructure. SEM cross-section analysis showed a hybrid selective layer with a thickness dependent on the sol precursor concentration.

## 2.1 Introduction

Membrane applications can result in a significant energy reduction for industrial applications like in the areas of biofuels [1] and organic solvents recovery [2, 3]. However, for several separation applications, the membranes must overcome the desired selectivity and permeability trade-off as well as to achieve high stability and reliability under reactive operating conditions. Membranes that possess a microporous-structure (pore size < 2nm) can separate molecules either by molecular sieving or by affinity of specific molecules with the membrane material. When the pore size distribution of the porous structure is almost similar to the size of smallest molecule, this molecule can be separated from larger ones by simple molecular sieving. Generally, the term molecular sieving in membranes is used when the membrane pore size is < 1nm.

Acid catalyzed sol-gel derived silica membranes (pore size approximately 0.3 nm) are favorable candidates for gas separation due to their high thermal stability, high porosity and unprecedented performance. Sol-gel processing brings a strong possibility of controlling the pore structure of silica membranes and allows an ultra-thin coating of few tens of nanometers with high hydrogen permeance and performance [4]. These membranes are preferred over membranes developed by other techniques like chemical vapor deposition (CVD) due to ease of fabrication and higher H<sub>2</sub> permeance ( $2 \times 10^{-6}$  mol/m<sup>2</sup>.s.Pa [4]) than for CVD derived membranes (H<sub>2</sub> permeance in the order of  $10^{-8}$  mol/m<sup>2</sup>.s.Pa [5]). However in wet conditions, the silica structure collapses due to hydrolysis of Si-O-Si groups, resulting in a reduced performance of the membrane.

The use of organic-inorganic silica alkoxides, such as *bis* (triethoxysilyl) ethane (BTESE), which contains organic groups between two silicon atoms, as a precursor, has demonstrated several times to be applicable for pervaporation and gas permeation [6-10]. The presence of a hydrocarbon group in this precursor brings the essential stability for these membranes under harsh industrial conditions but lacks the thermal stability at elevated temperatures (i.e. at 600 °C) in comparison to silica membranes due to the presence of organic groups inside the membrane matrix [6]. Castricum et. al [6] have shown that these type of hybrid silica membranes can be exceptionally stable in alcohol dewatering applications at

elevated temperatures. In gas separation, the commercial viability of these membranes is yet to occur due to poor  $H_2/CO_2$  and  $H_2/CH_4$  permselectivity. Another approach to modify the porous membrane microstructure for specific gas separation is the use of dopants like niobia in the BTESE matrix [11]. It is shown that niobia doping has improved  $H_2/CO_2$  permselectivity to above 700. The author claims that niobia contents create acid sites in the membrane matrix that resulted in a very low  $CO_2$  permeance through the membrane.

Although high hydrogen permeance values through BTESE membranes have been reported by Tsuru et. al [7], these membranes also show excessive permeance of  $SF_6$ , raising serious concerns about the uniformity in the pore size distribution and/or the presence of (micro-) defects in the membrane separation layer. A careful control and a critical check on sol process parameters (i.e. hydrolysis ratio, acid ratio, precursor concentration, reaction time) can give us more insight in sol morphology development during sol synthesis and in this way a better control in membrane formation can be achieved.

The BTESE sol synthesis strategy involves in most cases a multi-step addition of reagents with long sol processing (condensation) times (around 6-8 hours) [7, 8]. It is assumed that addition of any reagent during sol processing results in discontinuities during the reaction, which might complicate reaction kinetics, and may produce inhomogeneous sols and consequently inhomogeneous membrane characteristics (morphology, pore-size distribution etc.). Besides, with long sol condensation times, it is very likely that the sol particles might aggregate. Besides, in the sol-gel membrane fabrication process, dip coating is one of the most critical steps for the formation of the selective layer formation, followed by drying and calcination. Multi-step dip-coating, which is often used in literature, results in a multi-layered structure with thicker selective layers that can be more selective but will show lower permeances [12].

In this paper a simple and relatively fast approach for developing BTESE hybrid sols is described. All reactants could be added in one single step giving a monodispersed polymeric sol with particles of suitable size, which, after deposition on a multi-layered structure via a single dipping procedure, produces membranes with effective gas permselectivity results. The sol rheology was fine tuned to make the sols adaptable for a defect-free (no  $SF_6$  permeance) selective layer. The effect of sol

reaction time on membrane microstructure has been studied, and implications of sol rheology in producing membranes with sufficient H<sub>2</sub>/CH<sub>4</sub> permselectivity are presented in this contribution.

## 2.2 Experimental

As precursor 1,2-*bis*(triethoxysilyl)ethane (BTESE) (purity 97%, ABCR Germany) was used. Water was deionized at 18.2 MΩ/cm using a Millipore purification system. A polymeric sol was prepared by drop-wise adding BTESE to a nitric acid (65%, Aldrich) water-ethanol mixture. Addition was done in an ice-bath under vigorous stirring to control pre-mature (partial) hydrolysis. This mixture was refluxed at 60°C for either 1.5 or 3 hours under continuous stirring to produce hybrid sols. The effect of several process parameters i.e. precursor concentration [Si], hydrolysis ratio (HR), defined as hydrolysable ethoxy groups i.e. [H<sub>2</sub>O]:[OC<sub>2</sub>H<sub>5</sub>], and acid-precursor ratios (AR) [H<sup>+</sup>]:[Si], was studied to produce defect-free membranes.

Disc-shaped α-alumina supported γ-alumina membranes (pore size 3-5 nm) were prepared by a dip-coating procedure of a boehmite sol on α-alumina supports (support thickness of 2.08±0.01 mm and pore diameter of 100nm; Pervatech B.V. The Netherlands), followed by subsequent drying and calcination, as described in detail in [4]. The boehmite-PVA dip-sol was twice coated on α-alumina supports to develop a smooth mesoporous intermediate layer. A pore size for the γ-alumina intermediate layer of 3-5nm was determined by permporometry, using the method as described in [13].

Dip-coating of a BTESE sol (with dipping speed of 1.4 cm/sec) on γ-alumina membranes was done in a cleanroom class 1000 to minimize defect formation due to dust particles. The dipping procedure was performed only once to deposit the selective hybrid layer on the mesoporous support. After coating of the hybrid sol, the membranes were calcined at 300°C for 3 hours under nitrogen flow (99.99% pure), applying heating and cooling rates of 0.5 °C/min.

The sol and membrane fabrication experiments were performed several times to confirm the reproducibility of these results.

Particle sizes of freshly prepared hybrid sols were determined by dynamic light scattering (DLS) using a Malvern Zetasizer Nano ZS at 25°C. The viscosity of the sols

with several [Si] was determined by a rolling ball viscometer (Anton Paar, Belgium) at 25°C. The thickness of the calcined hybrid silica layers was determined by analyzing cross-sectional views of the membranes using a high-resolution scanning electron microscope HR-SEM (ZEISS 1550) at an accelerating voltage of 2.0kV.

Membrane characterization was performed on an in-house designed single gas permeation (SGP) set-up in a dead-end mode without backpressure. The membranes were sealed in a stainless steel module using Viton® 51414 O-rings with the separation layer exposed to the feed side. The gas permeance was measured at 200°C in a sequence, starting with the gas of smallest kinetic diameter, from He (0.255 nm), H<sub>2</sub> (0.289 nm), N<sub>2</sub> (0.364 nm), CO<sub>2</sub> (0.33 nm), CH<sub>4</sub> (0.389 nm) to SF<sub>6</sub> (0.55 nm) and H<sub>2</sub> (again) at 200°C with a trans-membrane pressure of 2 bar. The H<sub>2</sub> permeance measurements were performed again at the end of all measurements to ensure stable membrane microstructure. Only a 1 - 3 % variation in H<sub>2</sub> permeance was observed between the two measurements. The gas permeation results of each Si concentration were reproduced four times.

Membrane performance via SGP was determined by:

$$F_i = \frac{N_i}{\Delta P} \quad (1)$$

Where F is the permeance of gas *i*, determined by calculating the molar flux (N) of the gas through the membrane at a pressure difference (ΔP) between feed and permeate side.

## 2.3 Results and Discussion

### 2.3.1 Hybrid Silica Membrane Fabrication

A first indication whether a sol is suitable for membrane fabrication is that it must not gelate during the sol synthesis. Thus, a careful control of sol process parameters (Si concentration, AR, HR) was critical in obtaining a non-gelated BTESE sol. In membrane fabrication, control of sol particle size determines the quality of coated layer. The particle size of developed sols must be in a range that, when deposited on mesoporous intermediate layer, the sol should form a homogenous and smooth selective layer. Deposition of sols with particle sizes smaller than the mean pore size

of the porous support will result in sol infiltration and coating with a too large polymeric sol leads to a thick layer that is prone to crack formation [6, 14].

In this work, BTESE sols were produced starting with Si concentrations of 0.9 M and 1.8 M. A sol, prepared with a Si concentration of 0.9 M, produced systems with an average particle size of 4 nm. The particle size of these sols was of the same order of magnitude as the pore size of the  $\gamma$ -alumina intermediate layer. A test of the membrane after coating/calcining with a rhodamine solution showed a bare  $\gamma$ -alumina surface, indicating that no dense hybrid layer was formed on the top of the  $\gamma$ -alumina. Therefore the Si concentration was increased to 1.8 M to obtain larger sol particles in order to avoid sol infiltration in the membrane support, resulting in a homogeneous layer after coating. It is possible that a Si concentration between 0.9 M and 1.8 M can also produce BTESE sols with the desired particle size and morphology, but in the current work the Si concentration of 1.8 M was further investigated for finding optimal experimental conditions for reproducible fabrication of BTESE hybrid membranes.

Table 2.1 represents BTESE sol fabrication recipes at a Si concentration of 1.8 M, a reaction time of 1.5 hours and a reaction temperature of 60 °C. Different hydrolysis and acid ratios were used to produce sols. Acid ratios of 0.3 and 0.5 resulted in gelled sols at all hydrolysis ratios. It is observed [15] that higher acid contents accelerated cluster formation inside the sol, which forced sol aggregation and ended up in sol gelation. A higher acid ratio also leads to liquid-liquid immiscibility that disrupted reaction kinetics, also causing sol gelation. In the present work no liquid-liquid immiscibility was observed during the sol fabrication process, while only an acid ratio of 0.1 produced non-gelated sols at hydrolysis ratios of 1, 2 and 3 (table 2.1).

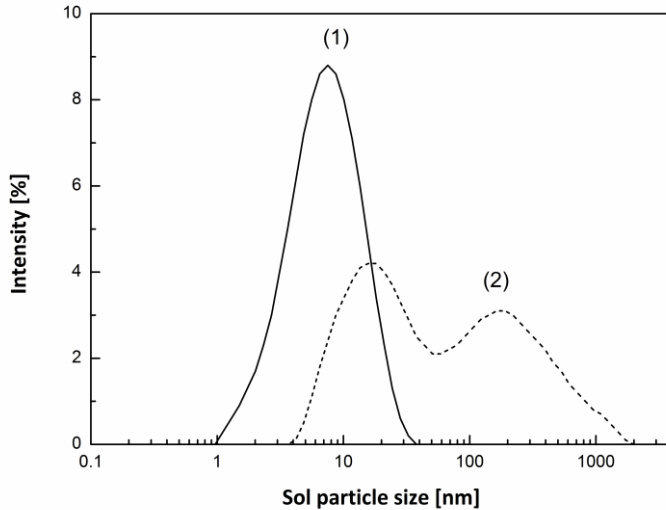
Chapter 2: Influence of sol-gel process parameters on the micro-structure and performance of hybrid silica membranes

**Table 2.1:** T = 60 °C, t = 1.5 h, Si = 1.8 M (BTESE = [Si / 2])

Acid Ratio [H <sup>+</sup> :Si]	Hydrolysis Ratio [H <sub>2</sub> O:OC <sub>2</sub> H <sub>5</sub> ]	Sol particle size and distribution after Sol processing
<b>0.1</b>	1	Monodisperse; Z* <sub>mean</sub> = 8 nm
	2	Very high polydispersity; Z <sub>mean</sub> > 40 nm
	3	Very high polydispersity; Z <sub>mean</sub> > 100 nm
	4	Sol gelation
<b>0.3</b>	1	Sol gelation
	2	Sol gelation
	3	Sol gelation
	4	Sol gelation
<b>0.5</b>	1	Sol gelation
	2	Sol gelation
	3	Sol gelation
	4	Sol gelation

Z\* = sol particle size

BTESE sols, produced at a Si concentration of 1.8 M, AR = 0.1 and HR = 1, were chosen for membrane coating because the average particle size of these sols was about 7-8 nm and it was the only sol with a uniform particle-size. This mother sol was called sol 1. To study the effect of reaction time on sol properties, another mother sol (sol 2) was synthesized under identical reaction conditions as sol 1, though with an increased reaction time of 3 hours. The increased reaction time produced a sol with a bimodal particle size distribution with relatively larger sol particles than sol 1 (as shown in figure 2.1).

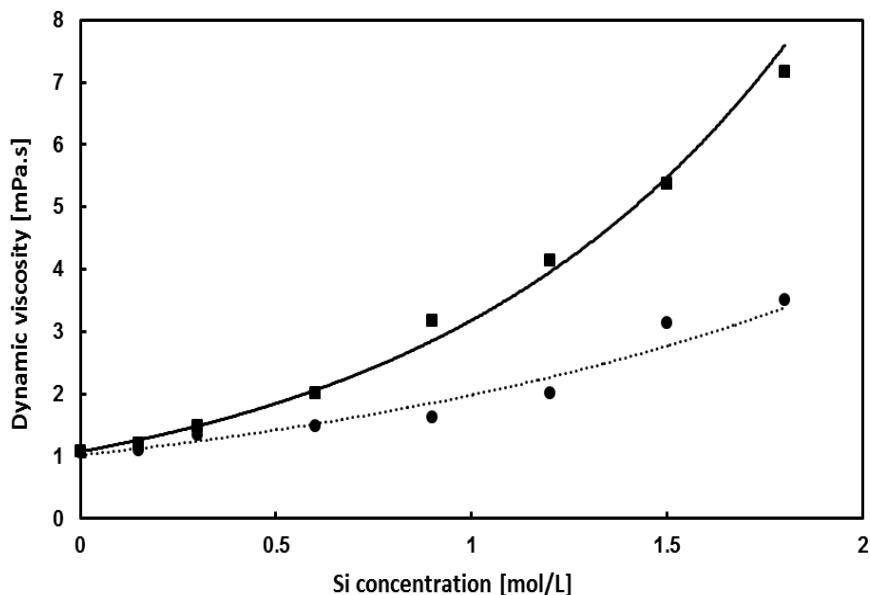


**Figure 2.1:** Particle size and particle-size distribution of sol 1 (1.5 hours) and sol 2 (3 hours), as determined by dynamic light scattering at 25°C.

Figure 2.2 shows the viscosity at 25°C of fresh mother sols 1 and 2 as a function of [Si], as achieved by diluting the respective sols with appropriate amounts of ethanol. It is clear from this figure that sol 2 shows a stronger increase in viscosity with increasing Si concentration if compared with sol 1. This can be explained by the fact that with an increase in reaction time, the extent of cross-linking between the sol particles (i.e. sol entanglement) increases resulting in an increase in sol viscosity [16]. The broad sol particle size distribution as observed for sol 2 can also be explained by this “sol-entanglement” effect. The particle size distribution in sol 1 is more uniform and its viscosity only slightly increases with increasing sol concentration. Since high viscous sols tends to gelate faster than the moderate ones [16] and the fact that this gelation plays a pivotal role in dip-coating and consequently in the development of a defect-free membrane, it is a pre-requisite that the sol must not have a too high viscosity. In general, viscous sols exhibit more slip effects than lower viscous sols at the same concentration and tend to form a non-uniform and thicker deposited layer [12]. Therefore the membranes developed by high viscous sols will be more prone to get cracked than those developed by



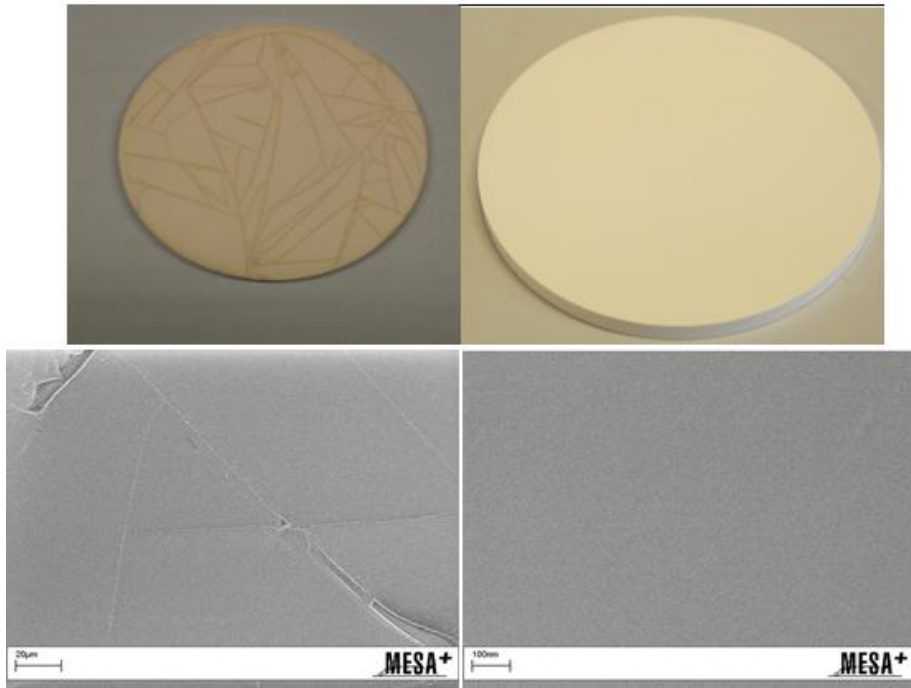
lower viscous sols. Besides, during drying and calcination of viscous dipped sols, the capillary forces of the gel (in the selective layer) can exceed the adhesion limit between support and gel, ending up in delaminating the selective layer completely from the substrate.



**Figure 2.2:** Sol viscosity at 25°C as a function of precursor concentration and varying sol processing time. ● (1.5 hours) and ■ (3 hours).

Figure 2.3 shows a 0.6 M crack-free membrane from sol 1 (right) and a 1.8 M cracked membrane from sol 2 (left) after calcination. The 1.8 M membrane of sol 2 was selected as illustration because of more visible surface cracks than other membranes. Crack-free BTESE membranes from sol 1 were produced at Si concentrations of 0.09 M, 0.15 M, 0.3 M, and 0.6 M respectively. If, by applying this sol 1, a concentration of more than 0.6 M was used, not all membranes remained crack free. Membranes produced from sol 2 only results in crack-free membranes at concentrations of 0.15 M and 0.3 M. Although there was a very small difference in sol viscosity between sol 1 and sol 2 at a sol concentration of 0.6 M (see figure 2.2), sol 1 gave crack-free membranes while sol 2 gave cracked membranes. This is due to the difference in sol particle size and morphology between sol 1 and sol 2 that

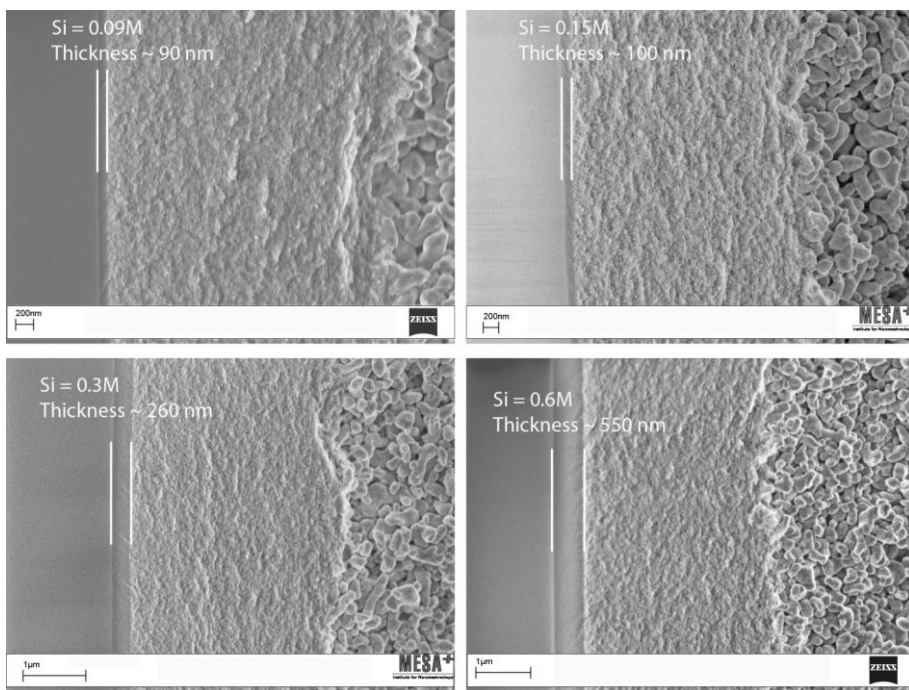
developed into a completely different pore-microstructure after dipping and calcination.



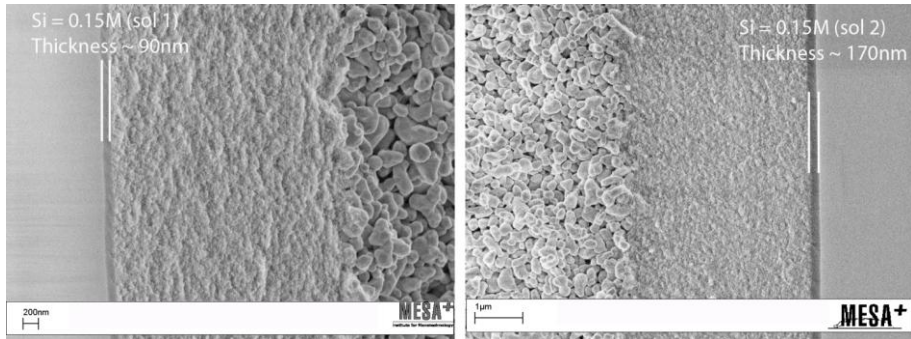
**Figure 2.3:** Surface of a disc-shaped cracked BTESE membranes (**left**) and crack-free membrane (**right**) after calcination at 300°C under nitrogen. **Left:** BTESE membrane from sol 2 with a Si concentration of 1.8 M; **Right:** BTESE membrane from sol 1 with a Si concentration of 0.6 M.

During calcination at high Si concentration the entangled network of the more viscous sol 2 increased the capillary forces between deposited particles, and destroyed the pore microstructure resulting in cracks on the membrane surface and eventually the top layer gets detached from the surface resulting in a complete breakdown in microstructure. Castricum et. al. [6] showed that membrane coating starting from polymeric sols with large particle sizes and high fractal dimensions lead to thicker membranes, which are prone to crack formation. Defects can be minimized by controlling the sol viscosity, withdrawing speed during dip-coating [17], and post dipping treatment procedure (calcination conditions like heating /cooling program, atmosphere etc.).

High resolution scanning electron microscopy was carried out to study the thickness of membranes made by both sols using various dipping concentrations. All membranes discussed in this part are defect free; i.e. no cracks were found by HR-SEM and no detectable permeance of SF<sub>6</sub> was observed (see later). Micrographs of membranes from sol 1 gave a sequential array of membrane thickness as a function of Si concentration, as shown in figure 2.4. Membranes with a Si concentration of 0.6 M have a membrane thickness of 550 nm while the membrane with a Si concentration of 0.09 M possessed a thickness of 90 nm. The membrane from sol 2 with a Si concentration of 0.15 M developed into a layer thickness of 170 nm (figure 2.5), which is almost twice as thick as a membrane from sol 1 with a similar Si concentration (90 nm: see figure 2.4). In conclusion, by controlling the sol viscosity and the particle size of the dip sols, an ultra-thin and homogenous selective layer can be produced.



**Figure 2.4:** Cross-sectional SEM micrographs of defect-free BTESE membranes developed from sol 1 with varying sol concentrations (degree of dilution).



**Figure 2.5:** Cross-sectional SEM micrographs of BTESE membranes made of sol 1 (left) and sol 2 (right) with an identical Si concentration of 0.15 M.

### 2.3.2 Hybrid Silica Membrane Performance

Single gas permeation (SGP) results of calcined BTESE membranes from sol 1 and 2 are shown in table 2.2 and 2.3 respectively. All membranes showed no  $\text{SF}_6$  permeance (detection limit of the equipment is  $5 \times 10^{-10} \text{ mol/m}^2 \cdot \text{s} \cdot \text{Pa}$ ), indicating a defect-free structure. It can therefore be concluded that the pore size of all the fabricated membranes (from both sol 1 and sol 2) was less than 0.55 nm (= kinetic diameter of  $\text{SF}_6$ ).

**Table 2.2:** Single Gas Permeation and selectivity results at 200°C of hybrid membranes produced from sol 1 at dip-sol concentrations: 0.09, 0.15, 0.3 and 0.6 M.

Gas Kinetic Diameter [nm]	Gas (0.09 M)		Gas (0.15 M)		Gas (0.3 M)		Gas (0.6 M)	
	Permeance ( $10^{-7}$ mol/m <sup>2</sup> .s.Pa)	Selectivity H <sub>2</sub> /X	Permeance ( $10^{-7}$ mol/m <sup>2</sup> .s.Pa)	Selectivity H <sub>2</sub> /X	Permeance ( $10^{-7}$ mol/m <sup>2</sup> .s.Pa)	Selectivity H <sub>2</sub> /X	Permeance ( $10^{-7}$ mol/m <sup>2</sup> .s.Pa)	Selectivity H <sub>2</sub> /X
He = 0.26	3.32	1.39	3.52	1.22	2.52	1.23	2.05	1.31
H <sub>2</sub> = 0.289	4.62	1	4.32	1	3.12	1	2.7	1
CO <sub>2</sub> = 0.33	1.24	3.7	1.19	3.6	0.8	3.9	0.46	5.8
N <sub>2</sub> = 0.364	0.44	10.5	0.34	12.2	0.23	13.5	0.13	20.8
CH <sub>4</sub> = 0.369	0.4	11.5	0.23	18.8	0.16	19.5	0.11	23.7
SF <sub>6</sub> = 0.55	*	∞	*	∞	*	∞	*	∞

\* Below detection limit of equipment i.e. below  $5 \times 10^{-10}$  mol/m<sup>2</sup>.s.Pa.

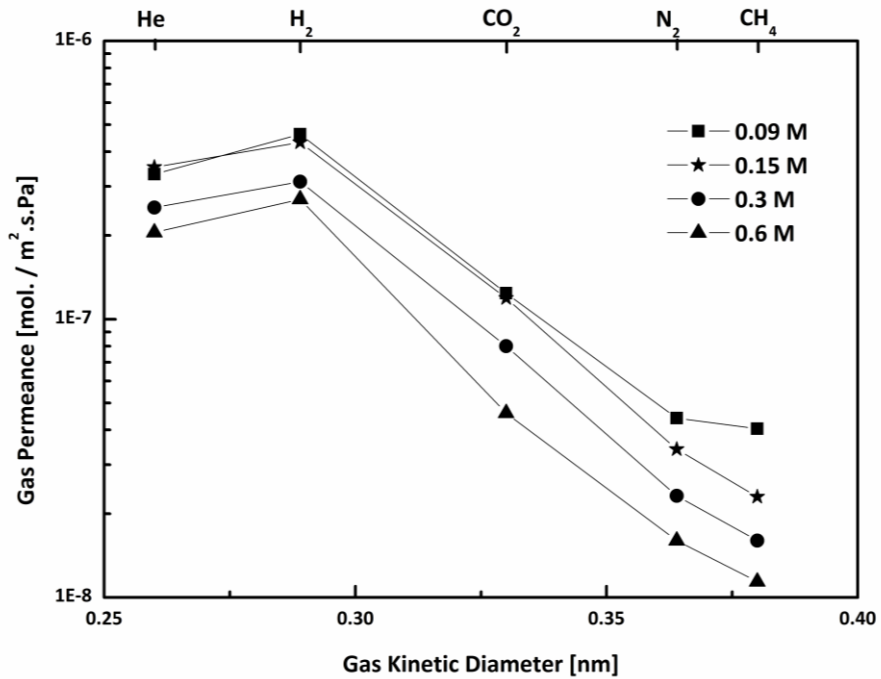
Chapter 2: Influence of sol-gel process parameters on the micro-structure and performance of hybrid silica membranes

**Table 2.3:** Single Gas Permeation and selectivity results at 200°C of hybrid membranes produced from sol 2 at dip-sol concentrations: 0.15 and 0.3 M.

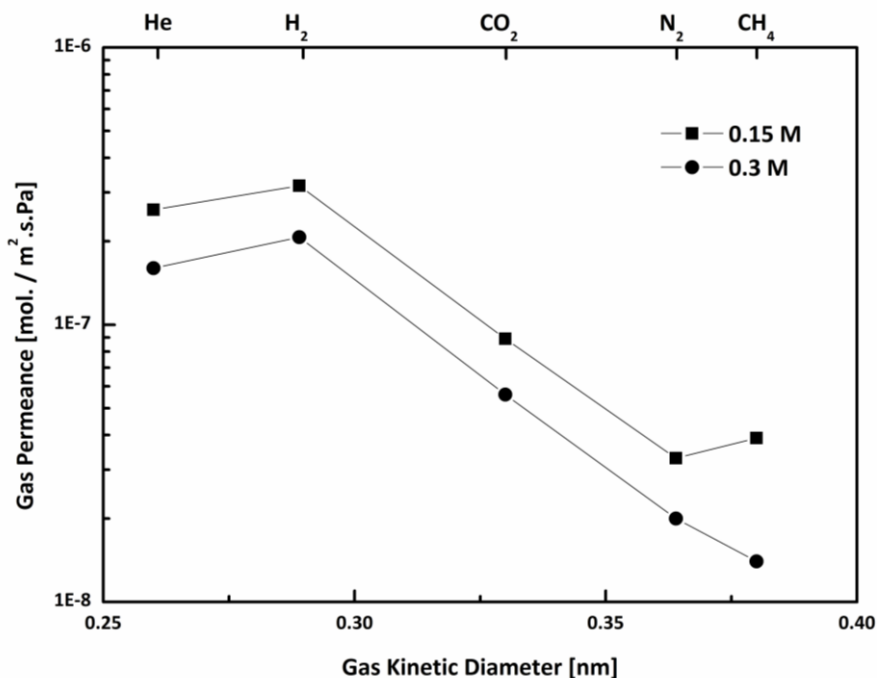
Gas Kinetic Diameter [nm]	Gas Permeance ( $10^{-7}$ mol/m <sup>2</sup> .s.Pa)	Selectivity	
		H <sub>2</sub> /X	H <sub>2</sub> /X
		(0.15 M)	(0.3 M)
He = 0.26	2.6	1.4	1.6
H <sub>2</sub> = 0.289	3.17	1	2.07
CO <sub>2</sub> = 0.33	0.89	3.7	0.56
N <sub>2</sub> = 0.364	0.33	10.2	0.2
CH <sub>4</sub> = 0.369	0.39	14.7	0.14
SF <sub>6</sub> = 0.55	*	∞	*

\* Below detection limit of equipment i.e. below  $5 \times 10^{-10}$  mol/m<sup>2</sup>.s.Pa.

Membranes developed from both sols showed for all gases a decrease in permeance with increasing dip-sol concentration (table 2.2 and 2.3). It elucidates that membranes prepared from a more diluted sol offered less gas flow resistance, but at the cost of H<sub>2</sub>/X selectivity. A H<sub>2</sub>/CH<sub>4</sub> selectivity of 24 was achieved (almost 10 times more than the Knudsen diffusion value of 2.8) with membranes made from sol 1 with a Si concentration of 0.6 M, while it was dropped to almost 12 with membranes made from sol 1 with a Si concentration of 0.09 M. Similarly, a H<sub>2</sub>/N<sub>2</sub> permselectivity of 21 was achieved with a Si concentration of 0.6 M which is almost 6 times more than the Knudsen selectivity of 3.7, indicating the molecular sieving effect of these membranes. All these results show that membrane performances were dependent on precursor concentration. Membranes developed by sol 2 at Si concentrations of 0.15 M and 0.3 M, show in most cases permeances as well as permselectivities lower than those made from sol 1, but still with H<sub>2</sub>/N<sub>2</sub> and H<sub>2</sub>/CH<sub>4</sub> permselectivities higher than selectivities calculated from Knudsen indicating that also here the transport mechanism is dominated by molecular sieving. To conclude, all membranes studies in this work showed better H<sub>2</sub>/N<sub>2</sub> and H<sub>2</sub>/CH<sub>4</sub> permselectivities than obtained with only Knudsen diffusion.



**Figure 2.6:** Single gas permeance results as a function of gas kinetic diameter of BTSE membranes made by sol 1.



**Figure 2.7:** Single gas permeance results as a function of gas kinetic diameter of BTESE membranes made by sol 2.

For inorganic silica ( $\text{SiO}_2$ ) membranes the He permeance is higher than  $\text{H}_2$  permeance because for these membranes the transport mechanism is based on molecular sieving resulting in a He/ $\text{H}_2$  permselectivity larger than 1 [4]. Lower permeances for He than for  $\text{H}_2$  are expected if the pores in the membrane are larger than 0.3 nm, because in that case Knudsen diffusion is dominating for these small molecules (He having lower mass), resulting in a He/ $\text{H}_2$  permselectivity of less than 1. For all BTESE hybrid membranes, produced from sols 1 and 2, the He/ $\text{H}_2$  permselectivity was less than 1 (between 0.7 and 0.75) indicating that the average pore size was bigger than 0.3 nm i.e. the BTESE membrane pore size is larger than the pure silica membrane pore size. For pure silica a pore size of less than 0.36 nm was determined [4]. Combined with the non-detectable  $\text{SF}_6$  permeance ( $d_k = 0.55$  nm) through these BTESE hybrid membranes made us conclude that the membranes studied in this work, have a pore size ranging from 0.3 nm to 0.54 nm.



To the best of our knowledge, these are by far the best pure and undoped hybrid silica membranes developed with a  $H_2/CH_4$  permselectivity of 24 and an infinite  $H_2/SF_6$  permselectivity at 200°C. Results, as given in literature, dealing with gas permeation of BTESE-derived hybrid membranes observed some  $SF_6$  [7, 10] permeance indicating a relatively more open pore microstructure.

For porous membranes, the  $H_2/CO_2$  Knudsen permselectivity is 4.7. A deposited selective layer must show a  $H_2/CO_2$  permselectivity of more than 4.7 to inscribe its significance as a  $CO_2$ -selective membrane. The BTESE membranes developed in this work however showed  $H_2/CO_2$  permselectivities below Knudsen diffusion except only one with 0.6M Si concentration showing a  $H_2/CO_2$  permselectivity of about 6, which is also not sufficient for industrial application. Castricum et. al. [9] has demonstrated that hybrid silica membranes exhibits affinity towards  $CO_2$  that can be tuned by tailoring the bridged hydrocarbons chains in the silicon moieties. From our work we can conclude that the  $CO_2$  transport across BTESE derived membranes is dominated by surface diffusion and not by molecular sieving.

## Chapter 2: Influence of sol-gel process parameters on the micro-structure and performance of hybrid silica membranes

**Table 2.4:** Gas separation performances of BTESE membrane are compared with the silica and other state-of-the-art BTESE membranes.

Membrane (Calc. T / °C)	H <sub>2</sub> permeation [mol/m <sup>2</sup> .s.Pa]	Selectivity H <sub>2</sub> /N <sub>2</sub>	Selectivity H <sub>2</sub> /CH <sub>4</sub>	Selectivity H <sub>2</sub> /SF <sub>6</sub>	Reference
Silica 400	2 X 10 <sup>-6</sup>	70	> 500	Infinity	[4]
Silica 600	5 X 10 <sup>-7</sup>	infinity	infinity	Infinity	[4]
BTESE 300	2 X 10 <sup>-5</sup>	10	-	-	[7]
BTESE 250	1.3 X 10 <sup>-6</sup>	16	-	-	[9]
BTESE 300*	5.6 X 10 <sup>-6</sup>	22	-	25,500	[10]
BTESE 300	4.3 X 10 <sup>-7</sup>	21	24	Infinity	This work

\* Membrane that showed the best permselectivity results amongst the ones reported in the contribution.

## 2.4 Conclusions

Hybrid silica membranes with interesting gas permselectivity properties have been reproducibly prepared from a single-step sol-gel synthesis route, using an ethoxy-bridged silane (BTESE) as precursor. The resulting membrane obtained by a single dipping/calcining step, consists of organically bridged silica moieties and has a more open micropore structure than pure silica membranes. The fabrication protocol is optimized and has undergone substantial simplification which enables us to develop sols with a mono-disperse particle size distribution. Sol rheology and its variation with Si concentration was investigated and defect-free hybrid membranes with varying layer thicknesses, dependent on sol concentration, could be produced. A H<sub>2</sub>/CH<sub>4</sub> permselectivity of 24 was achieved with membranes having a precursor concentration of 0.6 M.

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## **Chapter 3**

# **Hybrid silica membranes with enhanced gas separation properties**

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Hammad F. Qureshi, Hessel L. Castricum, Arian Nijmeijer, Louis Winnubst, "Hybrid silica membranes with enhanced gas separation properties".

## Abstract

A reliable and reproducible sol-gel process is reported for the fabrication of highly size-selective microporous hybrid silica membranes by using 1,2-*bis* (triethoxysilyl)ethane (BTESE) as a precursor. The acid concentration and the condensation time were tuned to synthesize membranes with a constricted pore structure by using a single dipping procedure. Single gas permeation experiments, performed at 200 °C, showed that the developed membranes could be impermeable towards nitrogen and methane, while all membranes showed a H<sub>2</sub>/N<sub>2</sub> permselectivity of at least 50. The size selectivity is far better than of all other hybrid silica membranes developed to date. SEM cross-section analysis showed a thin hybrid layer of about 440 nm, an isotropic surface and a flawless microstructure.

### 3.1 Introduction

The separation and purification of molecular mixtures in the chemical industry consume substantial amounts of energy. To reduce fossil fuel consumption, efficient separation processes are needed to obtain high-grade products in food and pharmaceutical industries [1, 2], high quality pure water [3], and to remove or recover toxic or valuable components from industrial effluents [4]. Today, membranes are used on a large scale for the production of potable water, for cleaning industrial effluents, to recover valuable constituents in biomass fermentation [5, 6], as well as for bio gas upgrading [7, 8] and gas and vapor separation [9, 10]. Besides, membranes are also a key component in energy conservation and - storage systems [11], artificial organs [12] and drug delivery devices [13].

Amorphous silica is an attractive material for application in microporous inorganic membranes, because of its thermal stability and high gas separation selectivity [14]. Through acid catalyzed sol-gel processing of e.g. tetraethylorthosilicate (TEOS), it is relatively easy to develop a thin separation layer with a narrow pore size that is applied onto a support that provides mechanical strength [15]. After calcination of the dip coated sol-gel derived silica network a homogeneous membrane is formed [16] that allows the selective permeation of small molecules such as helium (kinetic diameter = 0.26 nm) and hydrogen (0.29 nm), while showing little or no permeation of the bigger molecules like nitrogen (0.36 nm) or methane (0.39 nm) [17]. However, the modest stability of the silica structure to water severely limits its application in many industrial processes that involve hydrothermal conditions [18]. Modification of the silica network with metal ions [19-22] or the use of hydrophobic silanes [23, 24] has been reported to improve the hydrothermal stability.

An even more effective way to improve the hydrothermal stability of silica-based membranes is by using organic-inorganic silicon alkoxides (silsesquioxanes) that contain an organic bridging groups between two silicon atoms [25-27], such as 1,2-*bis*(triethoxysilyl) ethane (BTESE). This hybrid silica material has shown stability in water up to several years in pervaporation studies [18, 25]. It was suggested from computer simulations that the size of the bridging groups limits the size-based gas permselectivity, as the structural units may allow some permeance of molecules of



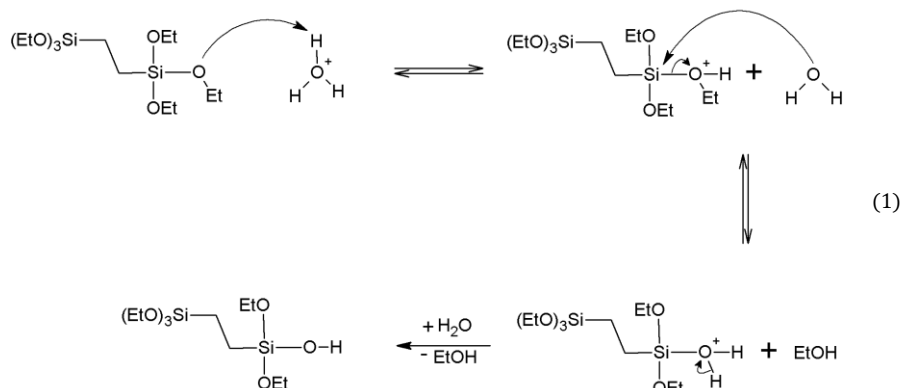
the size of N<sub>2</sub> [28, 29]. By using only BTESE as a silicon precursor, not only highly permeable hydrogen separation membranes can be successfully prepared [26], but also a homogenous and uniform pore-microstructure is possible by a single-dipping procedure resulting in a thin isotropic selective layer down to 90 nm thickness, showing a flawless pore microstructure [30]. However, no H<sub>2</sub>/N<sub>2</sub> and H<sub>2</sub>/CH<sub>4</sub> permselective ratios higher than 25 have yet been reported for these BTESE-derived membranes.

In a previous contribution we studied BTESE membranes prepared from acid-catalyzed sols using an acid ratio (AR, [H<sup>+</sup>:Si]) of 0.1, a hydrolysis ratio (HR, [H<sub>2</sub>O:OC<sub>2</sub>H<sub>5</sub>], where –OC<sub>2</sub>H<sub>5</sub> are the hydrolysable alkoxy-groups in the Si-precursor) of 1 and a precursor concentration [Si] of 1.8 M [30]. It is well-known that acid-catalyzed synthesis results in sols with linear polymer chains [17] which give microporous materials after drying and calcination. Reduction of the acid concentration results in lower hydrolysis and condensation rates [31]. In this work, BTESE sols are synthesized at a reduced acid ratio of 0.01. It was anticipated that this would lead to more constricted pores, and improve the size selectivity to gases.

## 3.2 Experimental

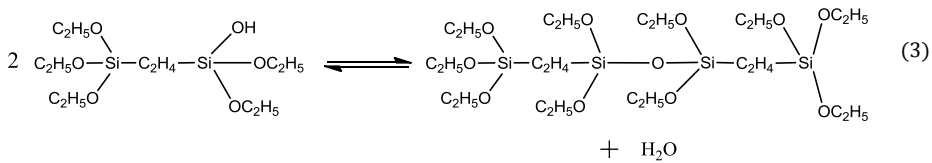
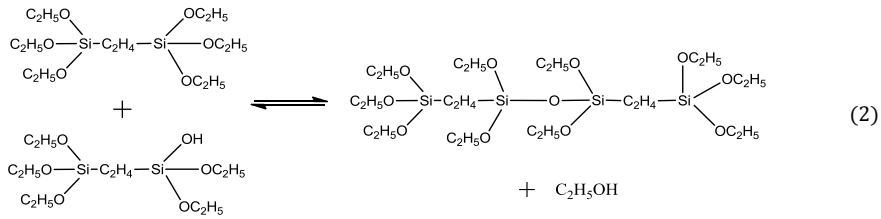
As a hybrid silica precursor 1,2-*bis*(triethoxysilyl) ethane (BTESE) (purity 97%, ABCR Germany) was used. Water was deionized at 18.2 MΩ/cm using a Millipore purification system. A polymeric sol was prepared by drop-wise addition of BTESE to a nitric acid (65 wt.%, Aldrich)–water–ethanol mixture. Addition was done in an ice bath under vigorous stirring to control pre-mature (partial) hydrolysis. This mixture was subsequently refluxed at 60 °C for 30 minutes under continuous stirring to produce hybrid silica sols at an acid ratio AR = 0.01, hydrolysis ratio HR = 1, and [Si] = 2.7 M. The molar ratio of added reagents was BTESE/EtOH/HNO<sub>3</sub>/ H<sub>2</sub>O of 1/4.6/6.8/0.02 respectively.

The acid catalyzed BTESE sol synthesis is expected to follow the same S<sub>N</sub>2-reaction mechanism as is observed for the synthesis of tetraethoxysilane (TEOS)-based sols [31-33]. The hydrolysis reaction of the hybrid siloxane (BTESE) under the formation of a silanol, with the liberation of alcohol as a by-product, is shown in the following scheme (equation 1).



During the hydrolysis reaction, the alkoxide group is rapidly protonated, resulting in the withdrawal of electrons from the silicon atom and consequently making the Si atom more electrophilic and more likely to be attacked by water. This is followed by the detachment of alcohol from the substrate, making it a 'leaving group'. As a result of this  $S_N2$  mechanism, the hydrolysis reaction is fast and it decreases after the removal of one ethoxy-group, because less electron providing substitutes become available to stabilize the positive charge on silicon atom.

The condensation reaction already starts before completion of the hydrolysis reaction [32]. During condensation the protonation of the hydroxyl groups in the silanols results in oxo-bridged siloxane (Si-O-Si) groups. Condensation is initiated by protonation of either an ethoxy or hydroxy group, which makes the neighboring silicon atom more electrophilic. Then this silicon atom is attacked by another silanol group, which resulted in the formation of an oxo-bridge. Depending on whether an ethoxy or a hydroxyl group was protonated, either ethanol or water will be the leaving group of the primer silicon atom respectively. Therefore, the BTESE condensation reaction follows two possible routes: water and alcohol condensation which are given in equation 2 and 3 respectively. The initial condensation is fast and decreases, as less electron providing substituents are left to stabilize the positive charge of protonated group.



From these sols membranes were synthesized by means of coating these sols on porous  $\gamma$ -alumina ceramics. Disc-shaped  $\alpha$ -alumina supported  $\gamma$ -alumina was prepared by a dip coating procedure of a boehmite sol on  $\alpha$ -alumina supports (support thickness of  $2.08 \pm 0.01$  mm and pore diameter of about 100 nm; Pervatech B.V. The Netherlands), followed by subsequent drying and calcination, as described in detail in [17]. The boehmite-PVA dip-sol was twice coated on  $\alpha$ -alumina supports in order to create a smooth mesoporous intermediate layer. A pore size for the - alumina intermediate layer of 3-5 nm was determined by permporometry, using the method as described elsewhere [34].

For membrane fabrication, the BTESE sol was diluted to a final dip-sol with  $[\text{Si}] = 0.6$  M. This BTESE separation layer was applied onto the alumina support by a single dipping procedure as described elsewhere [30], followed by a thermal treatment at 300 °C for 3 h under nitrogen (99.99% pure) with a heating / cooling rate of 0.5 °C/min. The sol and membrane fabrication experiments were performed several times to confirm the reproducibility of the results. The hybrid sol was synthesized three times and at least two membranes were produced from each sol and were characterized to validate the proof of concept.

Particle sizes of freshly prepared hybrid sols (with 75% dilution in ethanol) were determined by dynamic light scattering (DLS) using a Malvern Zetasizer Nano ZS at 25°C. The hydrodynamic diameter of the sol particles was determined from the

Brownian motion of the particles as defined by the translational diffusion coefficient  $D$  in the ethanol solvent. The hydrodynamic diameter  $d$  was obtained by the Stokes-Einstein equation:

$$d = kT / 3\pi\eta D \quad (4)$$

Where  $k$  = Boltzmann's constant;  $T$  = the temperature;  $\eta$  = solvent viscosity;  $D$  = diffusion coefficient in the solvent.

The thickness of the calcined hybrid silica layers was determined by analyzing cross-sectional micrographs of the membranes acquired with a high-resolution scanning electron microscope HR-SEM (ZEIS 1550) at an accelerating voltage of 1.0 kV.

Membrane performance was characterized on an in-house designed single gas permeation (SGP) set-up in a dead-end mode without back pressure. The membranes were sealed in a stainless steel module using Viton® 51414 O-rings with the separation layer exposed to the feed side. The gas permeance was measured at 200 °C in a sequence, starting with the gas of smallest kinetic diameter, from He (0.255 nm), H<sub>2</sub> (0.289 nm), CO<sub>2</sub> (0.33 nm), N<sub>2</sub> (0.364 nm), CH<sub>4</sub> (0.389 nm) to SF<sub>6</sub> (0.55 nm) at 200°C with a pressure difference of 2 bar. After the measurement of the different gases, the hydrogen flux was determined again to ensure that no changes had occurred in the membrane (micro) structure during the measurements.

The membrane performance via SGP was determined by equation 5:

$$F_i = \frac{N_i}{\Delta P} \quad (5)$$

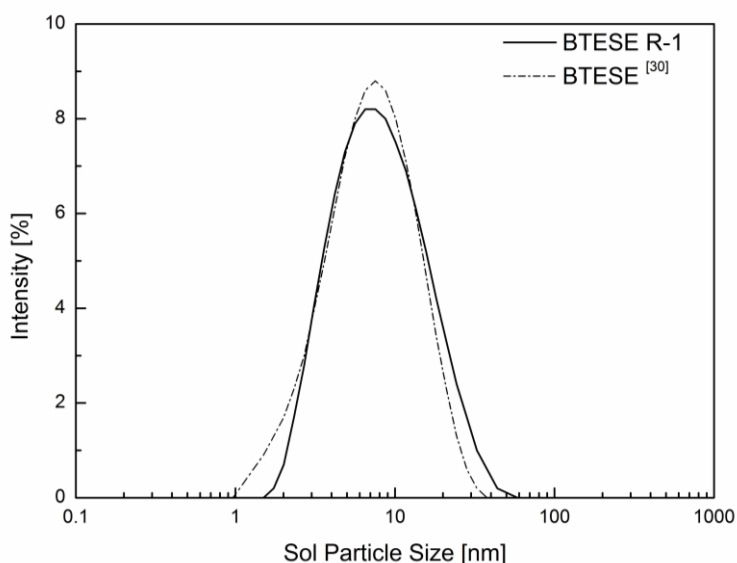
Where  $F$  is the permeance of the gas  $i$ , determined by calculating the molar permeance ( $N$ ) of the gas through the membrane with pressure difference ( $\Delta P$ ) between feed and permeate side.

### 3.3 Results and Discussion

#### 3.3.1 Sol-gel chemistry and fabrication of a hybrid silica membrane

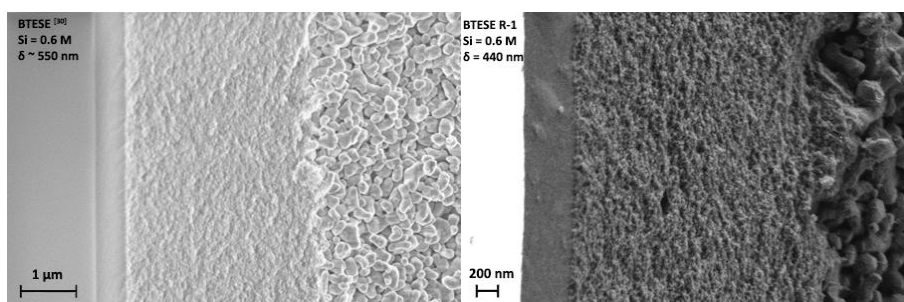
Sol synthesis is one of the most critical parts in the fabrication of meso and microporous ceramics for membrane applications. Therefore, the sol process parameters *i.e.* acid ratio  $[H^+:Si]$ , hydrolysis ratio  $[H_2O:OC_2H_5]$  and precursor concentration  $[Si]$  must be carefully controlled to obtain sols with appropriate particle size, morphology and homogeneity. The degree of homogeneity of the sols is crucial for obtaining a defect-free membrane pore-structure because coating with too large sol particles leads to thick layers that are prone to crack formation [30, 35].

In this work, sols from the BTESE precursor were prepared at a reduced nitric acid concentration compared with previous work [30] where a ten times higher amount of acid had been used to produce BTESE sols, *i.e.* at an acid ratio (AR) of 0.1. When sols with AR=0.01 were synthesized under the same experimental conditions, *i.e.* at 60 °C for 1.5 hours, the sol particle size was about 2 nm with a wide variation in size distribution. For microporous membrane fabrication, the sol particles must be larger than the pores of the ( $\alpha$ -alumina-supported) mesoporous  $\gamma$ -alumina supports, *i.e.* above 4 nm [35]. To synthesize larger sol particles, a higher precursor concentration was applied, *i.e.* at  $[Si]=2.7$ . This recipe was named "R-1". After 30 minutes at 60 °C, the sols acquired a mean particle size of about 7 nm with neat and uniform homogeneity as shown in figure 3.1. This size distribution is considered suitable for membrane preparation. At longer times, the sols were less suitable: the mean sol particle size after 1 hour and 1.5 hours were 12.5 nm and 13.7 nm respectively with high polydispersity. In figure 3.1, the sol particle size as obtained by sol recipe R-1, using a reaction time of 30 minutes, is compared with the sol particle size of BTESE as reported in [30], from which defect-free membranes had been prepared. While the lower AR of 0.01 resulted in decreased hydrolysis and condensation rates, this was compensated by a higher overall reactant concentration, keeping the reaction time within reasonable limits. Although the effect of the acid concentration could be further investigated, care should be taken that the conditions are still acid-catalyzed, *i.e.* below the isoelectric point, which is around pH=2 in an aqueous medium, as base-catalyzed systems (at pH > 2) may rather lead to a mesoporous structure.



**Figure 3.1:** Sol particle size distribution of BTESE R-1 sols . The sol particle size distribution is compared with results from [30].

A cross-sectional high resolution scanning electron micrograph (HR-SEM) of a membrane is shown in figure 3.2-(Right), indicating an isotropic thickness of about 440 nm of the BTESE separation layer on the  $\alpha$ -alumina support with a  $\gamma$ -alumina intermediate layer. This separation layer is about 100 nm thinner than a BTESE membrane developed from a sol prepared with an acid ratio (AR) of 0.1 and using an identical dip-sol concentration of 0.6 M [30] (figure 3.2-Left).



**Figure 3.2:** Cross sectional SEM-micrograph comparison of BTESE membranes developed with identical dip-sol concentration of 0.6 M. **Left:** BTESE membrane with AR 0.1 [30] with a

selective layer thickness of about 550 nm. **Right:** BTESE derived hybrid silica membrane developed from modified sol recipe R-1 (AR 0.01) with a selective layer of 440 nm.

### 3.3.2 Membrane Performance

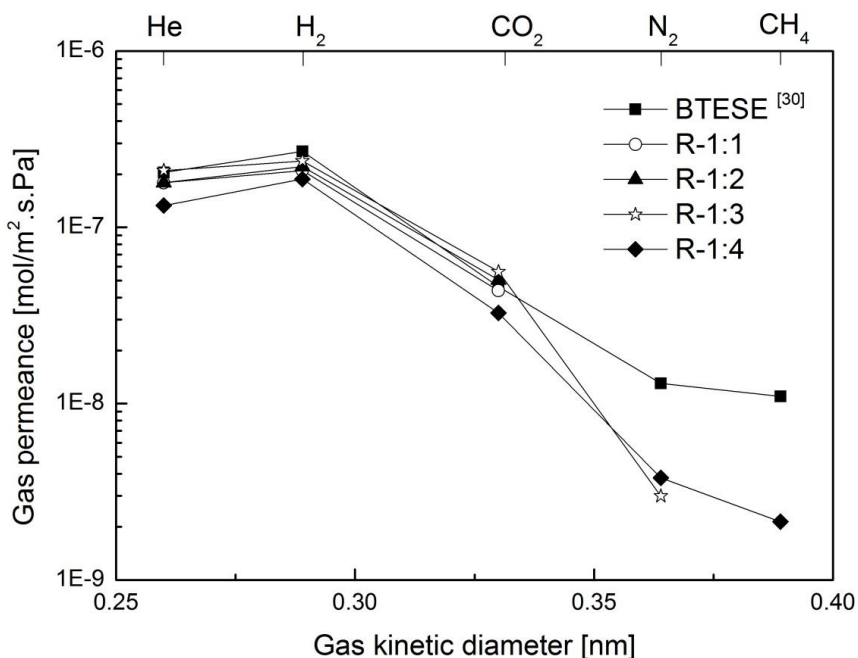
Single gas permeation (SGP) results of calcined hybrid silica (BTESE) membranes, reported in [30] at AR = 0.1 and membranes made by the modified R-1 method (with AR = 0.01) described in this work, are given in table 3.1 and in figure 3.3. At 200 °C none of the membranes showed SF<sub>6</sub> permeance (detection limit of the equipment is 5 X 10<sup>-10</sup> mol/m<sup>2</sup>.s.Pa) indicating a flawless microstructure. Two of the four synthesized R-1 membranes were found nitrogen and methane impermeable, while for the third membrane, there was no detectable methane permeance and a N<sub>2</sub> permeance of 3 X 10<sup>-9</sup> mol/m<sup>2</sup>.s.Pa, giving a H<sub>2</sub>/N<sub>2</sub> permselectivity of 80. A fourth membrane showed H<sub>2</sub>/N<sub>2</sub> and H<sub>2</sub>/CH<sub>4</sub> permselectivities of respectively 50 and 88. All these results are far superior in performance when compared with membranes starting from sols, prepared with an acid ratio (AR) of 0.1 (see table 1 and Fig 2). It should also be noted that the isotropic selective hybrid layer of the R-1 derived sol is 440 nm thick (Fig. 3), while the other BTESE derived selective layer has a thickness of 550 nm [30]. The permeance values for the smaller gases He, H<sub>2</sub> and CO<sub>2</sub> were found slightly lower, while permeances of bigger gases (N<sub>2</sub>, CH<sub>4</sub>) were reduced considerably for R-1 derived membranes. In general, by reducing the selective layer thickness gas permeances increase, which is in contrast with the results as discussed in this work. Furthermore, gas permeance of helium and nitrogen are comparable which strongly indicates that the pore microstructure by the R-1 method (AR 0.01) is more dense and homogenous, making it more difficult for bigger gas molecules to permeate through these membranes if compared with membranes made from sols, fabricated at higher AR [30].

**Table 3.1:** Single gas permeation results of BTESE membranes synthesized from sol recipe R-1 at an acid ratio AR=0.01, compared to those synthesized at AR=0.1 (\*) [30].

	Gas Permeances [mol/m <sup>2</sup> .s.Pa]					Permselectivity [-]					
	He	H <sub>2</sub>	CO <sub>2</sub>	N <sub>2</sub>	CH <sub>4</sub>	H <sub>2</sub> /He	H <sub>2</sub> /CO <sub>2</sub>	H <sub>2</sub> /N <sub>2</sub>	H <sub>2</sub> /CH <sub>4</sub>	CO <sub>2</sub> /CH <sub>4</sub>	
1.79E-07	2.10E-07	4.37E-08	-	-	-	1.2	5	∞	∞	∞	
1.79E-07	2.21E-07	5.03E-08	-	-	1.2	4	∞	∞	∞		
2.10E-07	2.38E-07	5.61E-08	2.99E-09	-	1.1	4	80	∞	∞		
1.33E-07	1.88E-07	3.27E-08	3.79E-09	2.14E-09	1.4	6	50	88	15		
2.05E-07*	2.70E-07*	4.60E-08*	1.30E-08*	1.10E-08*	1.3*	6*	21*	24*	4*		

- Below detection limit of equipment i.e. below  $5 \times 10^{-10}$  mol/m<sup>2</sup>.s.Pa.





**Figure 3.3:** Single gas permeation of all BTESE-based membranes developed from recipe R-1 (AR=0.01) and those of a BTESE membrane reported in [30] with AR=0.1.

A lower hydrogen permeance, a thinner selective layer, and better permselectivities with BTESE R-1 membranes, when compared with our previous findings [30], made us convince that there is a significant effect of reducing the acid concentration during sol fabrication on the final membrane microstructure. The pore structure has become more constricted and in some cases the membranes were found nitrogen impermeable. The least performing membrane, made by this method showed a H<sub>2</sub>/N<sub>2</sub> permselectivity of 50, which is still far better than observed with BTESE derived membranes made from a sol, using an acid ratio of 0.1 (i.e. H<sub>2</sub>/N<sub>2</sub> of 21) [30]. The findings can be of relevance for industrial application, not only for the separation of H<sub>2</sub>, but also for CO<sub>2</sub>/CH<sub>4</sub> separation in natural gas exploitation. Also in view of their excellent hydrothermal stability, BTESE-based membranes may find increased application in bio-and natural-gas separation and purification.

### 3.4 Conclusions

An efficient procedure to polymerize hybrid silica sols is reported that developed into high-performance membranes. Reducing the concentration of acid catalyst from 0.3 to 0.02 moles during the sol synthesis resulted in a notable influence on the membrane microstructure. The effectiveness of low acid concentration during the sol processing step was delicately utilized in developing high performance gas separation membranes. The condensation reaction is faster but by reducing its time we have developed monodispersed sol particles that formed a constricted pore microstructure. It has not only reduced the sol processing time to one-third (*i.e.* 30 minutes) from hybrid silica, but also the developed membranes showed an improved hydrogen permselectivity performance for bigger gases (*i.e.* H<sub>2</sub>/N<sub>2</sub> and H<sub>2</sub>/CH<sub>4</sub>) with a selective isotropic layer thickness of 440 nm. Further investigation of the structural development during sol synthesis and coating could enhance understanding of the processes that results in pore structures with very small pores. More insight in these sol-gel processes may lead to further improvement of the size selectivity of BTESE-based hybrid silica membranes for gas separation.

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## **Chapter 4**

### **Doped microporous hybrid silica membranes**

## Abstract

Hybrid silica (*i.e.* *bis*-triethoxysilyl ethane: BTESE) membranes doped with B, Ta or Nb, were made through a sol-gel process. Triethyl borate (TEB), tantalum (V) ethoxide (TPE), and niobium (V) ethoxide (NPE) were selected as doping precursors. The doping concentration was optimized to produce sols suitable for membrane fabrication. Thermal stability, structural analysis, cross-sectional micrographs and single gas permeation experiments were performed for doped-BTESE membranes and results are compared with an undoped BTESE membrane. It was observed that the synthesized doped-BTESE materials and membranes resulted into a more open (and, in one occurrence, SF<sub>6</sub> permeable) pore microstructure showing high permeances of larger gas molecules, while having a cross-sectional thickness comparable to un-doped BTESE membranes.

## 4.1 Introduction

Inorganic membranes have attracted considerable attention for their applicability in gas separation processes in conditions where polymeric membranes cannot be used. Inorganic membranes remain stable at high temperature (*i.e.* > 400 °C), do not swell in solvents, and are resistant to abrasion [1, 2]. Porous inorganic membranes with either size and/or affinity based selectivity offer potential advantages in separating gaseous mixtures at elevated temperatures [3], in catalytic membrane reactors [4] and in hydrogen separation [5]. The application of microporous silica membranes for hydrogen purification has been subject of study for a long time [4]. These membranes are either prepared by a chemical vapor deposition (CVD) technique [6, 7] or by using sol-gel methods [8-10]. Although silica membranes, fabricated by sol-gel methods, show great promise in gas separation, the technical challenges such as hydrothermal stability are still a point of concern [11]. Hybrid organosilica (e.g. *bis*-triethoxysilylethane: BTESE) membranes are very suitable to overcome such problems, since they show an improved hydrothermal stability [12, 13]. The exposure of silica to moisture (or steam) at around 70 °C leads to the hydrolysis of Si-O-Si bonds [1]. The introduction of organic bridges in the silica microstructure makes it less susceptible for hydrolysis which extends the industrial application of silica membranes [14]. It has been reported that the shape, flexibility and length of organic bridges in the hybrid silica network have an influence on the membrane pore size, structure and affinity [15].

For a gas permselective membrane the pore size and pore size distribution should be small and sufficiently uniform to ensure that the membrane acts as an efficient sieve to block larger gas molecules for permeating through the membrane. The presence of hydrocarbon chains in the silica backbone improves the hydrothermal stability of such a hybrid silica matrix however at the cost of reduced gas selectivity [11]. A possible approach to improve the gas permselectivity of these hybrid silica membranes is the incorporation of metal-ions in the hybrid silica matrix. This approach was successfully implemented by doping the silica network with metal ions, such as aluminum and magnesium [16], zirconium [17, 18], niobium [19, 20], nickel [21] and cobalt [22, 23]. For hybrid silica (*i.e.* BTESE) only the incorporation of niobia was reported to date [24, 25], where it is claimed that the introduction of niobia created surface active sites resulting in a reduced CO<sub>2</sub> permeance. These



authors observed that the  $H_2/CO_2$  permselectivity at  $450^\circ C$  was higher (*i.e.*  $H_2/CO_2 = 220$ ) compared to hydrogen selectivity over larger molecule such as nitrogen ( $H_2/N_2 = 125$ ) and thus claiming that  $CO_2$  permeance through these Nb-BTESE membranes was not only determined by size exclusion. However, in the same work, this enhanced  $H_2/CO_2$  permselectivity was not observed at  $300^\circ C$  and  $350^\circ C$  [ $(H_2/CO_2)_{300^\circ C} = 11.4$ ,  $(H_2/CO_2)_{350^\circ C} = 11$ ,  $(H_2/CO_2)_{400^\circ C} = 50$ ;  $(H_2/N_2)_{300^\circ C} = 50$ ,  $(H_2/N_2)_{350^\circ C} = 45$ ,  $(H_2/N_2)_{400^\circ C} = 65$ ] which raises questions regarding niobia incorporation, its influence on reduced  $CO_2$  permeance and the reproducibility in fabrication of Nb-BTESE membranes. Because of this inconsistency in results a new study on Nb-doped BTESE was performed as described in this chapter.

Furthermore, we report the incorporation of boron and tantalum in the hybrid silica (BTESE) matrix with the aim to fabricate a defect-free, gas selective membrane film. Boron has extensively been used as a glass forming agent due to their low thermal expansion coefficient. In membrane fabrications, Boron was doped in a silica matrix using boric acid powder as boron source to reduce the defect density and enhance the membrane performance [26]. The Si-C-C-Si bond strength of hybrid silica is unknown but in silica, Si-O has a bond strength of 368 KJ/mol [27] and the bond B-O strengths are respectively 560 KJ/mol and 790 KJ/mol for  $BO_4^-$  and  $BO_3$  species respectively [27]. The incorporation of boron in the hybrid silica matrix was expected to bring more rigidity and tightness to hybrid silica matrix. In this research triethylborate (TEB) is used as a boron source for doping the hybrid silica matrix.

Tantalum is known for its high chemical and hydrothermal stability and belongs to the refractory metal group [28]. Thin films of tantalum oxide are already in use in transistors [29], sensors [30], and capacitors [31]. It has been reported that sol-gel derived ultra-thin tantalum membranes resulted in a dense structure with very low hydrogen permeance [32]. On the other hand, hybrid silica membranes possess a relatively loose pore microstructure [33]. In the current work, tantalum is used as a dopant in hybrid silica, to form a relatively denser microstructure than that of undoped BTESE [33] for improved  $H_2/X$  gas permselectivities.

## 4.2 Experimental

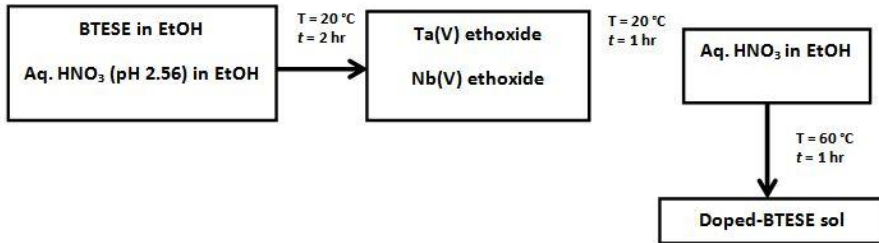
As hybrid silica precursor 1,2-*bis*(triethoxysilyl) ethane (BTESE) (97%, ABCR Germany) was used. Triethyl borate [TEB] ( $B(OC_2H_5)_3$ ), 99%, Aldrich), niobia (V) ethoxide [NPE] ( $Nb(OC_2H_5)_5$ , 99.99%, ABCR Chemicals) and tantalum (V) ethoxide [TPE] ( $Ta(OC_2H_5)_5$ , 99%, ABCR Chemicals) were respectively used as boron, niobium and tantalum source.

For the synthesis of boron doped hybrid silica (B-BTESE) sols the following procedure was used. Triethyl borate (2.51 ml) was added to a BTESE-ethanol mixture (11.10 ml BTESE in 6.38 ml ethanol) in a round bottom flask. Into that flask, a mixture of nitric acid (0.5 ml, 65 wt.% Aldrich), water (3.65 ml, deionized) and ethanol (15.85 ml, Absolute, Aldrich) was added under vigorous stirring in an ice-bath. The solution was kept at 60 °C for 1.5 hr. The sol contained 20 at% B ( $= [B]/[B + Si]$ ).

The hydrolysis step for the synthesis of tantalum-doped hybrid silica (Ta-BTESE) sols was performed in a glove box under nitrogen atmosphere. A solution of 0.495 ml nitric acid (pH 2.56) in 12.25 ml ethanol was added to a BTESE-ethanol mixture (3.26 ml BTESE in 9.44 ml ethanol) and stirred for 2 hrs at 20 °C. TPE (1.11 ml in 40.77 ml ethanol) was added to the aforementioned solution and the reaction was further allowed to run for 1 hr at 20 °C under constant vigorous stirring. Finally 0.43 ml nitric acid (pH 2.5) dissolved in 12.25 ml ethanol, was added to the doped-hybrid silica mixture and the reaction was allowed to run at 60 °C for another 1 hr. The Ta-BTESE hybrid sol contained 20% Ta ( $= [Ta]/[Ta + Si]$ ).

Niobium-doped hybrid silica (Nb-BTESE) sols were made by using the following reaction scheme. A solution of 0.46 ml nitric acid (pH 2.5) in 12.25 ml of ethanol was added to a BTESE-ethanol mixture (3.26 ml BTESE in 9.44 ml ethanol) in a glove-box under nitrogen atmosphere. The solution was stirred at 20 °C for 2 hrs. After that 1.05 ml NPE in 40.83 ml ethanol was added to the solution and the reaction was allowed to run for 1 hr at 20 °C under constant vigorous stirring. Finally 0.43 ml nitric acid, dissolved in 12.25 ml ethanol, was added to the solution and the reaction was allowed to run at 60 °C for 1 hr under reflux. The Nb-BTESE hybrid sol contained 20% Nb ( $= [Nb]/[Nb + Si]$ ).

Figure 4.1 presents a schematic description of the Ta-BTESE and Nb-BTESE sol synthesis procedure. If not applied immediately after synthesis, all doped-BTESE sols were stored at  $-28\text{ }^{\circ}\text{C}$ . For membrane dip-coating the sols were diluted 6 times with ethanol resulting in a final concentration of  $0.3\text{ M}$  ( $[\text{Si}] + [\text{M}]$ ).



**Figure 4.1:** Sol Fabrication scheme of niobia and tantalum doped BTESE sols.

Particle sizes of freshly prepared hybrid sols (with an extra 75% dilution in ethanol) were determined by dynamic light scattering (DLS) using a Malvern Zetasizer Nano ZS at  $25\text{ }^{\circ}\text{C}$ . Measurements were performed using 1.0-1.5 ml of the sol in a disposable size cuvette (Type DTS0012, Malvern Instruments).

Disc-shaped  $\alpha$ -alumina supported  $\gamma$ -alumina was prepared by a dip coating procedure of a boehmite sol on  $\alpha$ -alumina supports (support thickness of  $2.08 \pm 0.01$  mm and pore diameter of about 100 nm, Pervatech B.V. The Netherlands), followed by subsequent drying and calcination, as described in detail in [34]. The boehmite-PVA dip-sol was coated twice on the  $\alpha$ -alumina disc supports to create a smooth mesoporous intermediate layer. A pore size for the  $\gamma$ -alumina intermediate layer of 3-5 nm was determined by permporometry, using the method as described elsewhere [35].

For membrane fabrication, the separation layer was applied onto the  $\alpha$ -alumina supported  $\gamma$ -alumina by a single dipping procedure as described elsewhere [33], followed by a thermal treatment at  $300\text{ }^{\circ}\text{C}$  for 3 hr under nitrogen (99.99% pure) with a heating / cooling rate of  $0.5\text{ }^{\circ}\text{C}/\text{min}$ . The sol and membrane fabrication experiments were performed several times to confirm the reproducibility of the results.

The thickness of the calcined hybrid silica layers was determined by analyzing cross-sectional micrographs of the membranes, acquired from a high-resolution scanning electron microscope HR-SEM (Zeiss 1550) at an accelerating voltage of 1.0 kV.

Dried powders of doped-hybrid silica sols were obtained by drying the corresponding sols in a petri dish overnight at room temperature. These powders were analyzed using thermogravimetry (TGA). Measurements were carried out on a STA 449 F3 Jupiter<sup>®</sup> (Netzsch) instrument under nitrogen atmosphere. About 20 mg of sample was used and each measurement run from room temperature until at least 800 °C at a heating rate of 10 °C min<sup>-1</sup>.

FTIR spectra of calcined un-doped and doped-hybrid silica powders were obtained with a TGA-IR Tensor 27 system spectrometer (Bruker Optick GmbH) in the range 400-4000 cm<sup>-1</sup>, using a resolution of 4 cm<sup>-1</sup> and 16 scans.

Membrane performance was characterized on an in-house designed single gas permeation (SGP) set-up in a dead-end mode. The membranes were sealed in a stainless steel module using Viton<sup>®</sup> 51414 O-rings with the separation layer exposed to the feed side. The gas permeance was measured at 200 °C in a sequence, starting with the gas with the smallest kinetic diameter, from He (0.255 nm), H<sub>2</sub> (0.289 nm), CO<sub>2</sub> (0.33 nm), N<sub>2</sub> (0.364 nm), CH<sub>4</sub> (0.389 nm) to SF<sub>6</sub> (0.55 nm) at 200°C with a trans membrane pressure of 2 bar.

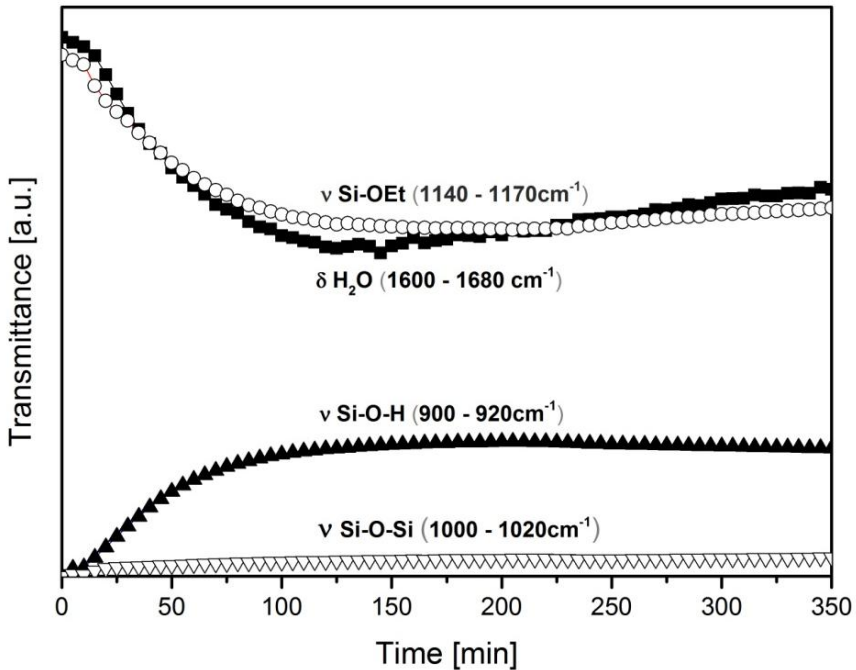
### 4.3 Results and Discussions

#### 4.3.1 Doped-BTESE sol characterization

The sol fabrication of B-BTESE was a relatively straight forward synthesis scheme. However, only 20% boron doping was possible for producing stable sols with appropriate particle sizes, necessary for membrane fabrication. Lower boron concentrations (*i.e.* 5%, 10%, and 15%) resulted in sol particles with an average size smaller than 4 nm with high polydispersity. 20% doping of TEB in BTESE showed to be sufficient to synthesize uniform bigger sol particles (of about 8 nm) which were applicable for membrane coating. It might be possible that more than 20% of TEB doping in the BTESE precursor during the sol synthesis would also lead to doped-

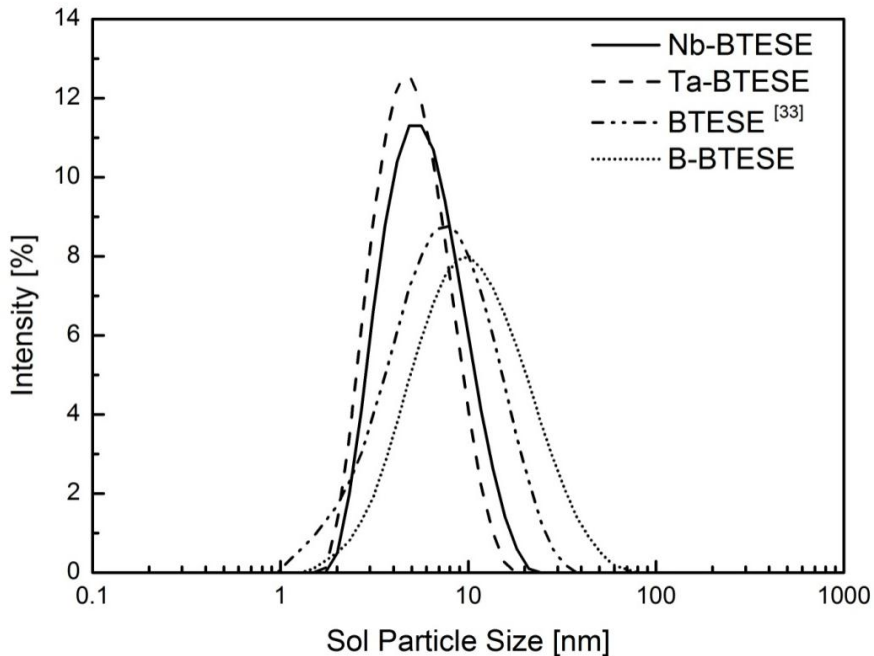
hybrid silica sols, suitable for membrane fabrication, but in this work a maximum of only 20% doping was employed.

During the synthesis of hybrid silica sols, containing the ethoxides of niobium or tantalum, by adding these ethoxides at the same time to the reaction mixture as the BTESE precursor, the system gelled within minutes, while a well-defined sol with a small and homogeneous particle size distribution was obtained for pure BTESE under identical synthesis conditions (*i.e.* temperature of 60 °C) [33]. As the reactivity of the tantalum and niobium precursors is very high, an alternative route was developed to control hydrolysis/condensation during sol-synthesis. This procedure not only resulted in the incorporation of these metal ion in the hybrid silica structure but also resulted in a homogenous sol particle size distribution with sizes slightly larger than (or equal to) the  $\gamma$ -alumina pore size of about 5 nm. Preliminary experiments confirmed that the metal precursors hydrolyze very fast, hence hydrolysis must be done under water lean conditions to enhance the possibility of their integration in the hybrid silica matrix. To investigate this, in-situ FTIR analysis was performed during the synthesis of a (undoped) BTESE sol at 20 °C. The evolution of different reactive groups and hydrolysis products as function of reaction time was examined by monitoring the changes in intensities of its specific IR vibration lines, as shown in figure 4.2. From this figure it can be observed that the intensities of the Si-O-Si remained relatively constant for an extended period of time. During the first 120 minutes of reaction the IR lines, corresponding to the BTESE ethoxy groups (SiOEt) as well as the one representative for (free) water decreased in intensity, while the intensity of the Si-OH vibration (corresponding to the hydrolysis product) increased simultaneously. After around two hours of reaction the free water line intensity increased slightly, which can be ascribed as a water condensation reaction where water is released as a by-product [9]. This FTIR analysis might not provide accurate information, but it gives an indication that hydrolysis of BTESE at 20 °C proceeds in 2 hrs. The combination of the lower amount of water in the reaction mixture and of already (partly) hydrolysis of BTESE after 2 hrs of reaction might sufficiently prevent the Nb- or Ta-alkoxide precursors from fast hydrolysis, and enhance the reaction of the metal ion with the BTESE hybrid silica precursor.



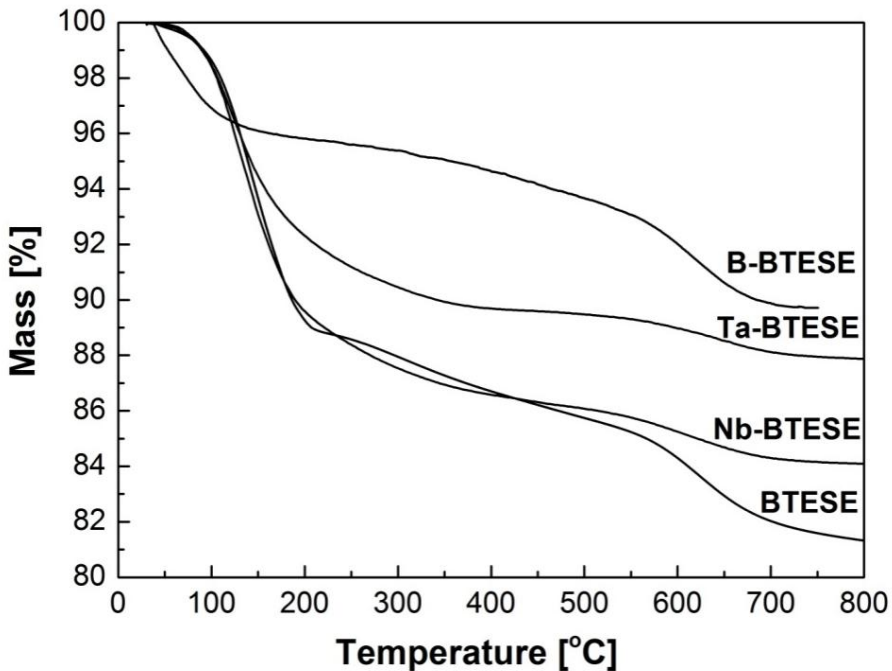
**Figure 4.2:** Variation in the transmittance intensity of IR-vibrations related with the hydrolysis of BTESE precursor at 20 °C.

The synthesis recipe was modified accordingly, in a way as shown in figure 4.1, to obtain a sol with uniform particle size and particle size distribution, applicable for membrane coating. BTESE and aqueous  $\text{HNO}_3$  were allowed to react inside a glove-box for 2 hrs at 20 °C as a pre-hydrolysis step before the addition of either Ta- or Nb-alkoxide. In this way the dopants are allowed to react with the hybrid silica matrix under water lean conditions, which is also suitable for a homogenous dispersion of the dopant in the hybrid silica matrix [36]. Finally, after 1 hr. the remaining nitric acid was added and the temperature was increased to 60 °C to ensure complete hydrolysis of all ethoxy groups and to facilitate the condensation process. This resulted in hybrid sols with high monodispersity and average particle size of about 6 nm for Ta-BTESE and about 7 nm for Nb-BTESE derived sols (figure 4.3).



**Figure 4.3:** Average sol particle size and size distribution of freshly synthesized doped-BTESE sols. The sol particle size is compared with undoped BTESE sol [33].

Figure 4.4 shows the TGA data of dried pure and doped-BTESE hybrid gels in nitrogen atmosphere. The color of the pure and all doped-hybrid silica gels changed from initially white into black or dark-brown after the TGA measurement, indicating pyrolysis of the samples during heating up to 800 °C. The continuous weight loss up to 200 °C for pure BTESE, Nb-BTESE and Ta-BTESE gels and up to about 150 °C for B-BTESE can be assigned to the evaporation of residual water and ethanol. After this evaporation step a slight weight loss is observed until 550 °C, which is assigned to a continuous decomposition (partial pyrolysis), followed by a stronger weight loss after 550 °C, which can be ascribed to the degradation of the ethylene bridge [37]. This weight loss observed at high temperature is more pronounced for the undoped and B-doped BTESE than for the Ta- or Nb-BTESE systems.



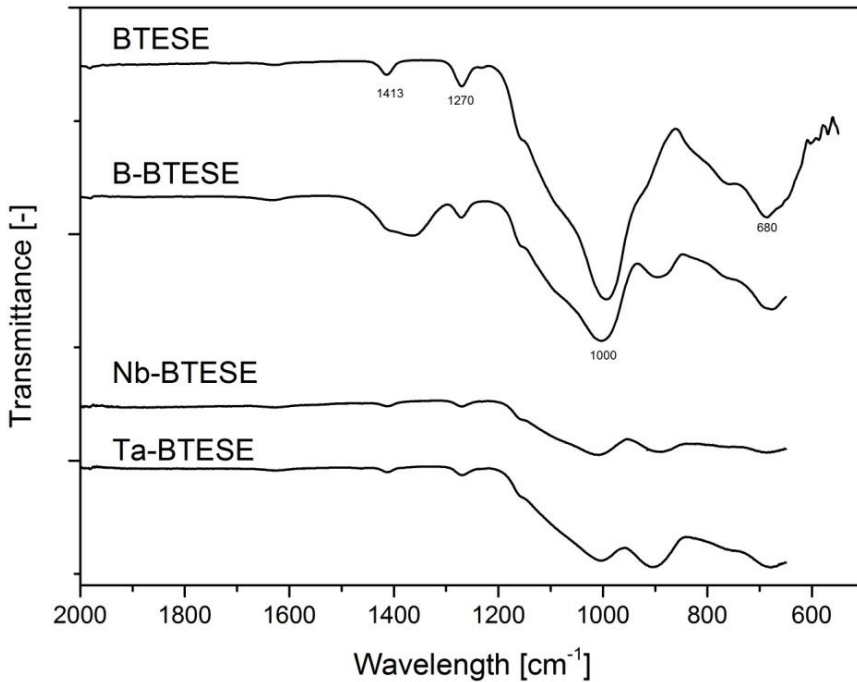
**Figure 4.4:** Thermo-gravimetric analysis (TGA) data of un-doped BTESE and doped (TEB, Ta and Nb) – BTESE dried gels recorded under nitrogen atmosphere.

No clear explanation is available in the literature about the onset of the degradation of  $-C_2H_4-$  in the hybrid silica precursor. In [37], it is claimed that the decomposition of the ethylene bridge in BTESE occurs between 480 °C and 800 °C in inert atmosphere. This is in good agreement with the results as depicted in figure 4.4. We can claim that a temperature of around 500 °C can be marked as a start of the degradation process of all doped- BTESE materials and that the hybrid system remains intact until 500 °C in an inert nitrogen atmosphere.

Figure 4.5 shows the FT-IR spectra of doped and undoped BTESE powders calcined at 300 °C under nitrogen atmosphere. For all samples  $CH_2$  vibrations at  $1270\text{ cm}^{-1}$  and  $1413\text{ cm}^{-1}$  [1, 38] are visible, which can be regarded as an evidence of the presence of  $Si-CH_2-CH_2-Si$  in these powders. The signals at  $1000\text{ cm}^{-1}$  and  $680\text{ cm}^{-1}$  are indicative for a  $Si-O-Si$  structure in the samples [38, 39]. The B-O stretching mode at  $1467\text{ cm}^{-1}$  is reported in literature for boron-silica systems [40]. However

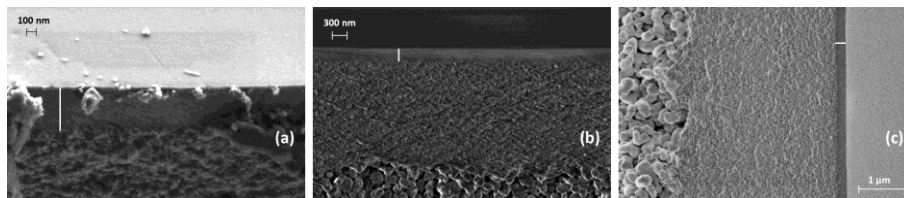


we were unable to find any proof of B-O in the hybrid silica matrix. For Nb-BTESE and Ta-BTESE, there was no indication either of any change in the hybrid structure by the inclusion of these elements, as also reported elsewhere [24]. From these results it can be concluded that all the dopants added to the BTESE did not disturb the hybrid silica network and that the central hinge of hybrid silica structure (*i.e.* ethylene bridge) is retained in all the doped-BTESE samples.



**Figure 4.5:** Fourier Transform IR spectra of un-doped and doped-BTESE powders after calcination at 300 °C.

Figure 4.6 shows cross-sectional HR-SEM micrographs of Nb-BTESE, Ta-BTESE and B-BTESE membranes. These membranes were fabricated using an identical dip-sol concentration of 0.3 M and an almost identical particle size distribution. Therefore any variation in thickness of the selective layer can be ascribed as an effect of doping to the hybrid silica matrix. The separation layers showed thicknesses of 360, 230 and 180 nm for respectively Nb-BTESE, Ta-BTESE and B-BTESE membranes. The undoped BTESE membrane formed a uniform selective layer of about 260 nm [33].



**Figure 4.6:** Cross-sectional HR-SEM micrographs of doped-BTESE derived membranes. **(a)** Nb-BTESE membrane with a selective layer thickness of about 360 nm, **(b)** Ta-BTESE derived with the selective layer thickness of about 230 nm, and **(c)** B-BTESE membrane with a selective layer thickness of about 180 nm.

### 4.3.2 Doped-BTESE membrane characterization

Single gas permeation experiments of Nb-BTESE, Ta-BTESE and B-BTESE membranes were performed at 200 °C. These results as well as those of undoped BTESE (taken from [33]) are given in table 4.1 and figure 4.7. In this way a judgment can be made over the pore size of these membranes.

The Nb-BTESE and Ta-BTESE membranes were impermeable to hexafluorosulfide ( $\text{SF}_6$ ) gas molecules which ensured that the pore size of these membranes was smaller than 0.55 nm. B-BTESE membranes showed some  $\text{SF}_6$  permeance which made us conclude that the B-BTESE membrane contains a few pores larger than 0.55 nm. The presence of pin-holes or defects in the selective layer was not visible by high resolution SEM and therefore it can be stated that the inclusion of boron, resulted in forming of relative larger pores when synthesized by sol-gel processing.

It was surprising to observe similar gas permeance values for all membranes because the B-BTESE membrane has a relatively thin selective layer if compared with the other doped and undoped BTESE membranes. The overall  $\text{H}_2/\text{X}$  gas permselectivity performance of all doped-BTESE membranes was less than for undoped BTESE membranes (see table 4.1). Nb-BTESE and Ta-BTESE membranes showed identical  $\text{H}_2/\text{N}_2$  and  $\text{H}_2/\text{CH}_4$  permselectivities. The incorporation of Nb and Ta in the hybrid silica matrix appears to form a similar pore microstructure but with a difference of almost 100 nm in the selective layer thickness. To enhance the selectivity of doped-BTESE membranes reported in this work, thermal treatment higher than 300 °C, or for much longer holding times than 3 hrs at 300 °C, could be

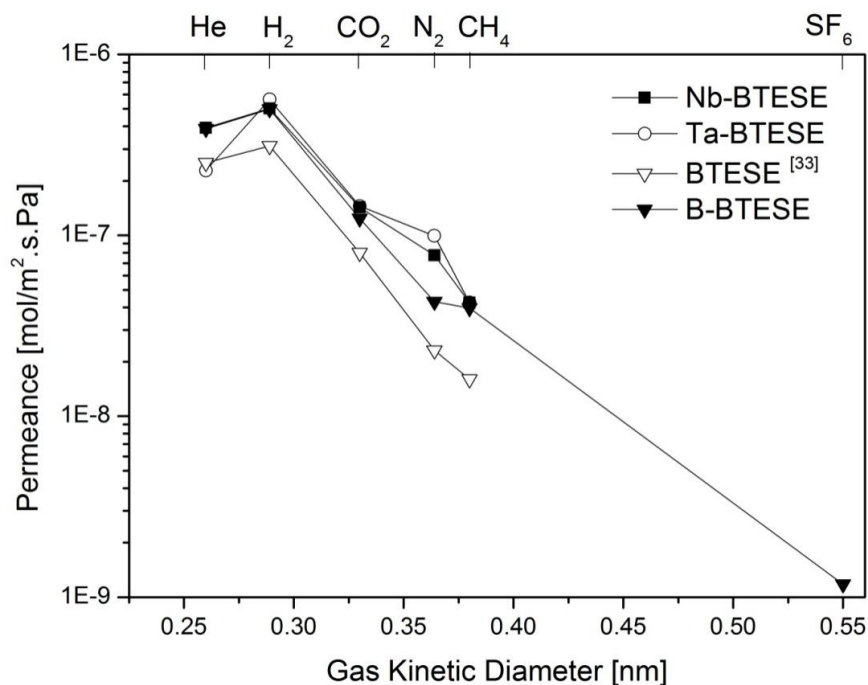
beneficial because the pore shrinkage due to thermal treatment might improve the gas permselective performance of these membranes. However, extreme care must be taken regarding the degradation of ethylene bridge. Although as it has been reported that the ethylene bridge might show a complete decomposition at 470 °C [37], it is not known yet at which temperature this degradation actually starts.

**Table 4.1:** Single Gas Permeation and permselectivity results at 200 °C of doped-BTESE developed with an identical dip-sol concentration. The results are compared with un-doped BTESE derived membranes [33].

<b>Gas Kinetic Diameter</b>	<b>Gas Permeance</b>	<b>Gas Selectivity</b>	<b>Gas Permeance</b>	<b>Gas Selectivity</b>	<b>Gas Permeance</b>	<b>Gas Selectivity</b>	<b>Gas Permeance</b>	<b>Gas Selectivity</b>
[nm]	(10 <sup>-7</sup> mol/m <sup>2</sup> .s.Pa)	H <sub>2</sub> /X	(10 <sup>-7</sup> mol/m <sup>2</sup> .s.Pa)	H <sub>2</sub> /X	(10 <sup>-7</sup> mol/m <sup>2</sup> .s.Pa)	H <sub>2</sub> /X	(10 <sup>-7</sup> mol/m <sup>2</sup> .s.Pa)	H <sub>2</sub> /X
	<b>BTESE [33]</b> <b>δ = 260 nm</b>		<b>B-BTESE</b> <b>δ = 180 nm</b>		<b>Ta-BTESE</b> <b>δ = 230 nm</b>		<b>Nb-BTESE</b> <b>δ = 360 nm</b>	
He = 0.26	2.52	1.23	3.88	1.28	4.06	1.39	3.92	1.28
H <sub>2</sub> = 0.289	3.12	1	4.98	1	5.65	1	5.03	1
CO <sub>2</sub> = 0.33	0.8	3.9	1.24	4	1.56	3.6	1.43	3.5
N <sub>2</sub> = 0.364	0.23	13.5	0.43	11.5	0.81	7	0.77	6.5
CH <sub>4</sub> = 0.369	0.16	19.5	0.39	12.7	0.46	12.3	0.42	12
SF <sub>6</sub> = 0.55	*	∞	0.01	500	*	∞	*	∞

Gas detection limit of equipment: 5 X 10<sup>-10</sup> mol/m<sup>2</sup>.s.Pa.

**6:** Thickness of the separation layer.



**Figure 4.7:** Single gas permeation analysis of Nb-BTESE, Ta-BTESE and B-BTESE derived membranes (calcined at 300 °C, with identical dip-sol concentration) as a function of gas kinetic diameter of permeating gas molecules measured at 200 °C. The results are compared with un-doped BTESE [33].

## 4.4 Conclusions

Three different membrane materials (B-BTESE, Ta-BTESE and Nb-BTESE) were fabricated by sol-gel processing and its applicability for gas separation was assessed by making microporous membranes, through a single dipping procedure. All the doped-BTESE sols formed a homogeneous selective layer of few hundreds of nanometers, as determined by high resolution SEM-micrographs. The structural evaluation by FT-IR spectroscopy of gels dried and calcined at 300 °C, indicated that the ethylene-bridge remains persistent in the silica backbone of BTESE for all systems. Single gas permeation analysis of Ta-BTESE and Nb-BTESE membranes indicated a defect-free pore microstructure with comparable H<sub>2</sub>/N<sub>2</sub> and H<sub>2</sub>/CH<sub>4</sub>

permselectivities of 7 and 12 respectively. The boron doped BTESE membranes had a relatively open pore microstructure that limits their application for gas separation applications. No effect of niobia doping on a decrease in CO<sub>2</sub> permeance was found, *i.e.* lower CO<sub>2</sub> permeance when compared with nitrogen and methane permeances, as observed by Qi et. al. [41] for some cases. It might be that either the claimed low permeances of N<sub>2</sub> and CH<sub>4</sub> are realistic or there could be experimental errors in the results presented by the author. To conclude, it is still unclear that incorporation of niobia in hybrid silica matrix would impart any significant effect in lower CO<sub>2</sub> permeance.

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## **Chapter 5**

**Metal-dispersed malonamide-bridged  
silsesquioxane precursors: Membrane  
fabrication and characterization**

## Abstract

To promote and facilitate dispersion of metal ions, such as  $\text{Ce}^{4+}$  and  $\text{Ni}^{2+}$ , within a hybrid silica matrix, a new hybrid silica precursor N,N,N',N'-tetrakis-(3-(triethoxysilyl)-propyl)-malonamide (TTPMA) has been successfully synthesized. The malonamide ligands coordinate the  $\text{Ce}^{4+}$  and  $\text{Ni}^{2+}$  metals and enhance their dispersion. Colloidal sols were successfully prepared from these metal-dispersed malonamide-bridged silsesquioxane precursors. After gelation and calcination the metal centers redistribute into small nanosized clusters of  $\text{CeO}_2$  (< 5nm) and  $\text{Ni}_2\text{O}_3$  (< 15nm). The sol-gel derived Ce-TTPMA and Ni-TTPMA membranes showed higher  $\text{H}_2/\text{N}_2$  and  $\text{H}_2/\text{CH}_4$  permselectivities than previously reported hybrid silica membranes. For Ce-TTPMA membranes, a 40% higher permselectivity for  $\text{H}_2/\text{N}_2$  and a 30% higher permselectivity for  $\text{H}_2/\text{CH}_4$  were observed. The Ni-TTPMA membranes were found nitrogen impermeable. The TTPMA-precursor can be a promising and versatile precursor for the incorporation of metal ions within hybrid silica matrices.

## 5.1 Introduction

The spectrum of membrane-based processes is extending and membranes can be employed for hydrogen separation in an industrial environment, oxygen enrichment for medical and industrial applications, natural gas purification, or in post-combustion carbon capture processes where CO<sub>2</sub> is separated from flue gases [1-5]. Currently, solvent-based absorption, using for example amines, is still the most commonly applied technique to capture CO<sub>2</sub>, but their regeneration requires a lot of energy, that somehow limitize their use in industrial separation processes [6-9].

The difference in kinetic diameter between H<sub>2</sub> and gases such as CO<sub>2</sub>, N<sub>2</sub> and CH<sub>4</sub> is very small (2.89 Å versus 3.30 Å, 3.64 Å and 3.89 Å respectively). However, these gases can be separated by size exclusion in silica membranes with a H<sub>2</sub>/CO<sub>2</sub> permselectivity of 70, while nitrogen and methane were found impermeable [10]. Due to the poor stability of these silica membranes in steam atmosphere metal-ions (i.e. cobalt or nickel) were added, in order to render membranes that preserve a high H<sub>2</sub> gas selectivity under hydrothermal conditions [11, 12]. Although inorganic, size-exclusion based, membranes will never exceed the hydrogen selectivity of palladium membranes, they are less expensive, catalytically inactive and do not suffer from hydrogen embrittlement and poisoning phenomena [13, 14].

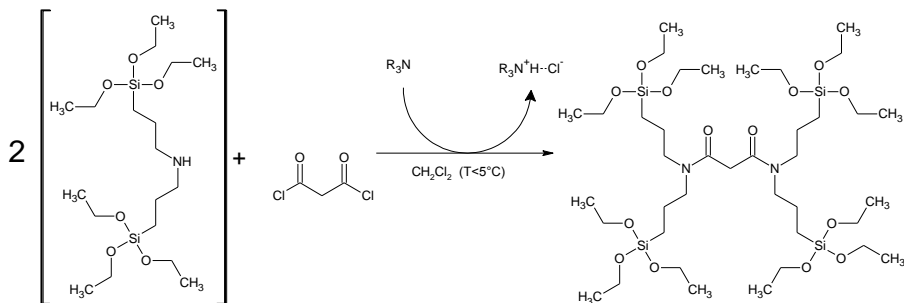
Dispersion of metals on an atomic scale into a hybrid silica network is not a straightforward task: the metal oxide that is introduced, either in the form of a metal salt or a metal alkoxide, tends to phase separate while the silica matrix is formed. Metal salts, e.g. metal nitrates, have limited solubility in the alcohols in which the silica sol is formed and these salts tend to precipitate while the sol is drying [12]. Metal alkoxides dissolve well in apolar solvents, but they are much more reactive towards hydrolysis and condensation than silica precursors, generally resulting in the formation of metal oxide clusters within the silica sol [15-17]. The reactivity of these alkoxides can be tempered by chelating ligands such as acetylacetone and they clearly retard the gelation in the presence of water [18-20].

In the present work, a bridged silsesquioxane precursor is studied, having four triethoxysilyl-propyl groups attached to a single malonamide chelating group. As compared to pendant silsesquioxanes, glasses or coatings made from bridged

silsesquioxanes exhibit much higher mechanical strength and fracture resistance due to enhanced connectivity and the absence of dangling carbon substituents [21-23].

A bridged silsesquioxane that consists of a malonamide chelating group was formed through the formation of amide bonds between malonyl chloride and two *bis*-(3-(triethoxysilyl)-propyl)-amine (TTPMA) molecules. The synthesis was performed via a base-catalyzed (using a tertiary amine as base) N-acylation of malonyl chloride on N-substituted amines in dichloromethane at temperatures below  $T = 5\text{ }^{\circ}\text{C}$  as reported before [24, 25] (see Figure 1). Malonamides are strong chelating units and through the formation of an enolic bidentate ligand they can easily form complex bonds with a large variety of metal cations, including lanthanides and actinides [26-33].

In this study, a hybrid silica precursor *N,N,N',N'*-tetrakis-(3-(triethoxysilyl)-propyl) malonamide (TTPMA) is developed consisting of a bridging malonamide group. This malonamide bridge can act as a chelating agent for the metal ions. Two metal ions i.e.  $\text{Ce}^{4+}$ , using cerium (IV) isopropoxide as a precursor and  $\text{Ni}^{2+}$ , using nickel nitrate precursor to investigate the metal-ions dispersion and membrane performance of metal-doped TTPMA. Ceria is reported as a catalyst in steam reforming of hydrocarbons and in water-gas shift reactions [34]. It is expected that a uniform dispersion of Ce inside the TTPMA matrix would result in a membrane with an enhanced affinity towards carbon dioxide leading to a higher  $\text{CO}_2/\text{CH}_4$  permselectivity. Nickel is used for hydrogen storage in fuel cells [35]. Ni was chosen as a doping material in a hybrid silica (TTPMA) matrix for metal dispersion and enhanced hydrogen permeance that is expected to result in its higher permselectivity against bigger gas molecules like nitrogen and methane.



**Figure 5.1:** Synthesis of N,N,N',N'-tetrakis-(3-(triethoxysilyl)-propyl)-malonamide (TTPMA).

## 5.2 Experimental

### 5.2.1 Synthesis of N,N,N',N'-tetrakis-(3-(triethoxysilyl)-propyl)malonamide (TTPMA)

Details on the synthesis of TTPMA are given in [36]. The solvents dichloromethane (BOOM, 99%), triethylamine (Sigma aldrich, 99%), and dimethylsulfoxide (Sigma Aldrich, 99%) were dried over anhydrous sodium sulphate (Sigma Aldrich, 99%). The synthesis was performed inside a glove box under nitrogen atmosphere. In a flask 30 mmol bis-(3-(triethoxysilyl)-propyl)-amine (ABCR chemicals, 97%) was dissolved in 183 ml dichloromethane. Subsequently, 30 mmol triethylamine was added to this solution. In a dropping funnel a 10 % excess (16.5 mmol) malonylchloride (Sigma Aldrich, 97%) was dissolved in 48.4 ml dichloromethane. This malonylchloride solution was drop-wise added in 30 min to the bis-(3-(triethoxysilyl)-propyl)-amine/triethylamine solution. After addition, the solution was stirred for 7 days at room temperature (*i.e.* at  $T = 20$  °C). After that, the dichloromethane was distilled using a Vacuubrand vacuum pump that automatically adapts its pressure to the solvent pressure. After completion of the reaction 150 ml hexane was used to extract TTPMA from the remnant slurry.

### 5.2.2 Ce-TTPMA and Ni-TTPMA Sol preparation, Membrane fabrication and Characterization

A stock-solution was prepared of approximately 3 mmol (1.28 g) of a cerium(IV) isopropoxide isopropanol adduct ( $[\text{Ce}(\text{O}^i\text{Pr})_4 \cdot i\text{PrOH}]$ : CeTiP; ABCR Chemicals, 31.5-

32.4% Ce by weight). A stoichiometric amount of TTPMA was added to this stock solution to yield a  $[\text{Ce}]/[\text{Si}+\text{Ce}]$  ratio of 1 : 10 (i.e. 10% Ce doping), which corresponded to  $[\text{Ce}]/[\text{TTPMA}] = 1/2.25$ . This mixture was diluted in 15 ml of isopropanol, yielding  $[\text{TTPMA}] = 0.29 \text{ mol/l}$  and  $[\text{Ce}] = 0.13 \text{ mol/l}$ . After stirring the solution for 24 h at room temperature (i.e. at  $T = 20 \text{ }^\circ\text{C}$ ), 13.29 ml of this Ce-TTPMA stock solution was further diluted in 16.71 ml isopropanol yielding 30 ml alkoxide solution with  $[\text{Ce-TTPMA}] = 1.8 \text{ mole/l}$ .

For the preparation of the Ce-TTPMA sol first a solution was prepared of 1.02 ml of 0.033 M  $\text{HNO}_3$  diluted in 28.98 ml isopropanol yielding a solution with:  $[\text{H}_2\text{O}] = 1.8 \text{ mol/l}$  and  $[\text{HNO}_3] = 0.06 \text{ mol/l}$ . This solution was added drop-wise to 30 ml of the diluted Ce-TTPMA precursor solution (prepared earlier), which yielded:  $[\text{OR}] = 0.9 \text{ mol/l}$ , where  $[\text{OR}]$  is the sum of ethoxy and iso-propoxy groups of TTPMA and  $\text{CeTiP}$  respectively. HR (hydrolysis ratio) =  $[\text{H}_2\text{O}]/[\text{OR}] = 1$ ,  $[\text{HNO}_3]/[\text{OR}] = 1/30$ ,  $[\text{TTPMA}] = 65.4 \text{ mmol/l}$  and  $[\text{Ce}] = 29.1 \text{ mmol/l}$ . The sol particles were formed by heating this solution for 1 hour at  $60 \text{ }^\circ\text{C}$ . For membrane preparation a 0.9 mol/l Ce-TTPMA sol was diluted 6 times by volume for membrane fabrication.

For the preparation of the Ni-TTPMA sol, first a  $\text{Ni}^{2+}$  solution was prepared by adding 10 g  $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  to 46 ml ethanol resulting in a solution with  $[\text{Ni}] = 0.691 \text{ mol/l}$ . This Ni solution and TTPMA were dissolved in ethanol to yield a diluted solution with  $[\text{Ni}]/[\text{Si} + \text{Ni}]$  ratio of 2:10 (i.e. 20% Ni doping) which corresponds to  $[\text{Ni}/\text{TTPMA}] = 1$ ,  $[\text{OR}] = 2.4 \text{ mol/l}$ ; where  $[\text{OR}]$  is the sum of ethoxy groups of TTPMA and the nitrate groups from nickel nitrate i.e.  $[\text{OR}] = [\text{NO}_3^-] + [-\text{OC}_2\text{H}_5]$ . After stirring for 2 h at room temperature, nitric acid was added drop wise to yield a sol with an acid ratio (AR)  $[\text{H}^+]/[\text{Si}] = 0.23$  and  $[\text{OR}] = 1.2 \text{ mol/l}$ . The hydrolysis ratio  $[\text{H}_2\text{O}]/[\text{OR}] = 1$  (including crystal water from the Ni solution) and complexing ratio  $[\text{Ni}]/[\text{TTPMA}] = 1$  were held constant. The sols were heated for 1 h at  $T = 60 \text{ }^\circ\text{C}$  while stirring.

Particle sizes of freshly prepared Ce-TTPMA and Ni-TTPMA sols were determined by dynamic light scattering (DLS) technique using a Malvern Zetasizer Nano ZS at  $25 \text{ }^\circ\text{C}$ . Prior to particle size analyses the sols were diluted 6 times with ethanol.

Fourier Transform Infra-Red (FTIR) measurements were performed by using a Bruker Tensor 27 equipped with a KBr beam splitter, a Pike GladiATR diamond

attenuated total reflectance (ATR) unit and a liquid nitrogen cooled MCT broadband detector. Samples of dried gels were applied on silicon wafers by spin coating and subsequently dried in air at 60 °C and calcined in nitrogen at 250 °C.

Disc-shaped  $\alpha$ -alumina supported  $\gamma$ -alumina membranes were prepared by a dip-coating procedure of a boehmite sol on  $\alpha$ -alumina supports (support thickness of  $2.08 \pm 0.01$  mm and pore diameter of 100 nm; Pervatech B.V. The Netherlands), followed by subsequent drying and calcination, as described in detail elsewhere [37]. The boehmite-PVA dip-sol was twice coated on  $\alpha$ -alumina supports to develop a smooth mesoporous intermediate layer. A pore size for the  $\gamma$ -alumina intermediate layer of 3-5nm was determined by permporometry, using the method as described in [38]. Dip coating of a Ce- and Ni-TTPMA sol (with dipping speed of 1.4 cm/sec) on  $\gamma$ -alumina membranes was done in a class 100 laminar flow cupboard, situated in a class 1000 clean room to minimize defect formation due to dust particles. The dip coating procedure was performed only once to apply the selective layer on the mesoporous support. After coating of the sol, the membranes were calcined at 250 °C for 3 hours under nitrogen flow (99.99% pure), applying heating and cooling rates of 0.5 °C/min.

The membrane performance was determined on an in-house designed single gas permeation (SGP) set-up in a dead-end mode without back pressure. The membranes were sealed in a stainless steel module using Viton® 51414 O-rings with the separation layer exposed to the feed side. The gas permeance was measured at 200 °C in a sequence, starting with the gas of smallest kinetic diameter, from He (0.255 nm), H<sub>2</sub> (0.289 nm), CO<sub>2</sub> (0.33 nm), N<sub>2</sub> (0.364 nm), CH<sub>4</sub> (0.389 nm) to SF<sub>6</sub> (0.55 nm) at 200°C at a trans membrane pressure of 2 bar. After the measurement of these gases, hydrogen flux was determined again to ensure that no change has occurred on the membrane (micro) structure due to permeation of several gases.

The membrane performance via SGP was determined by using the following equation;

$$F_i = \frac{N_i}{\Delta P}$$



Where  $F$  is the permeance of the gas  $i$ , determined by calculating the molar permeance ( $N$ ) of the gas through the membrane with pressure difference ( $\Delta P$ ) between feed and permeate side.

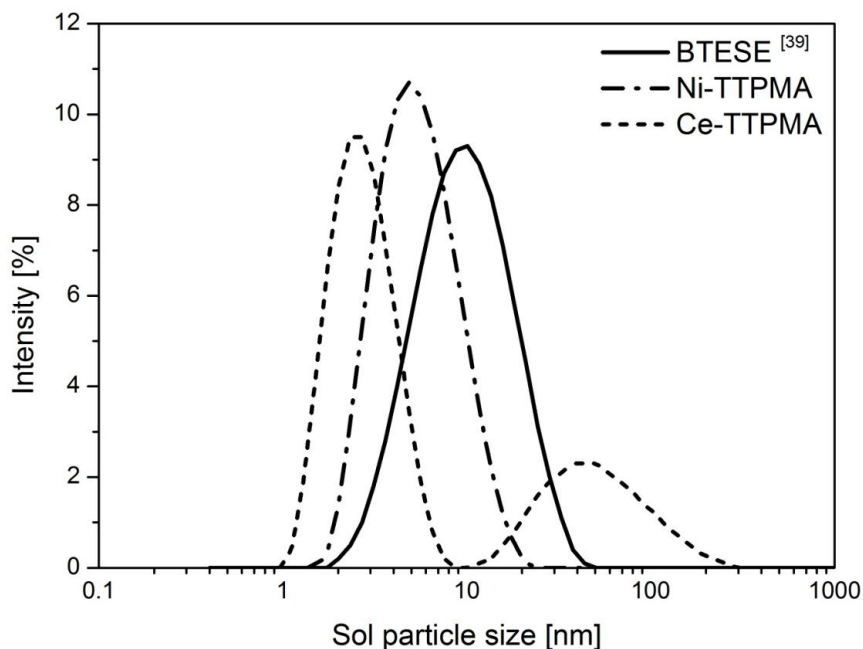
For Transmission electron microscopy (TEM) analysis carbon-coated TEM copper grids (CF200-Cu, Electron Microscopy Sciences) were dip-coated in undiluted Ni-TTPMA or Ce-TTPMA sols. The as-prepared films were dried at 60°C for 24 h and calcined at 250 °C under identical conditions as the calcination procedure used for calcination of the membranes. The samples were analyzed with a Philips CM300STFEG TEM at an accelerating voltage of 300 kV. Samples were investigated at low magnification to find typical areas and features of interest were examined at high magnification (GATAN 2048 Ultrascan1000 CCD camera).

Scanning electron microscopy (SEM) was performed on the cross-section of Ni-TTPMA and Ce-TTPMA membranes with a Zeiss Merlin HR-SEM using 1.4 kV acceleration voltage.

## 5.3 Results and Discussion

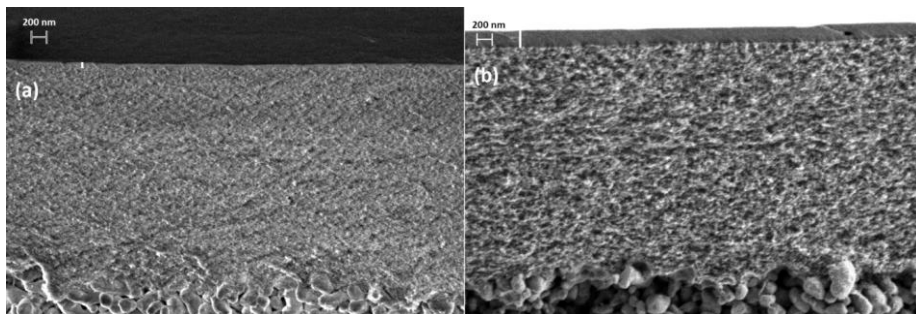
### 5.3.1 Sol and gel characterization

The sol particle size distributions of cerium and nickel doped TTPMA sol are shown in figure 2, together with the sol particle size distribution of a pure BTESE sol as described in [39]. The BTESE sol has an average particle size of about 7 nm. A Ni-TTPMA sol showed a mono-modal distribution curve with an average particle size of about 5 nm. The Ce-TTPMA sol showed a bi-modal size distribution with distinguishing average particle sizes of 2 nm and 40 nm respectively, while the Ni-TTPMA sol possessed a mono-modal size distribution with an average particle size of about 6 nm (as in figure 5.2).



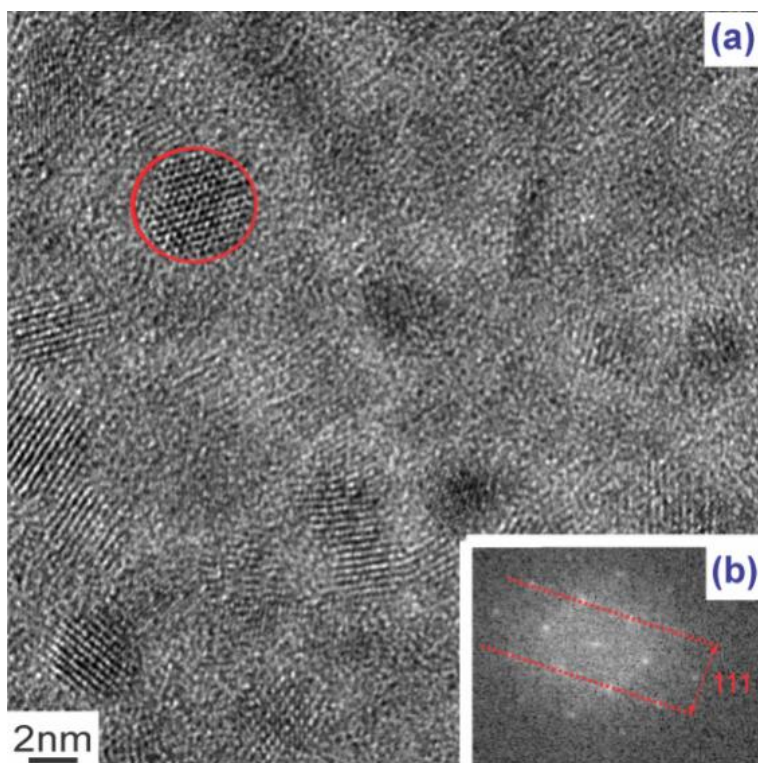
**Figure 5.2:** Sol particle size and distribution of Ce-TTPMA and Ni-TTPMA derived hybrid sols. The particle size and size distribution is compared with another hybrid precursor (BTESE).

High resolution cross-sectional SEM-micrographs of calcined Ce-TTPMA and Ni-TTPMA selective layers as deposited on  $\gamma$ -alumina are shown in Figure 5.3. The thickness of the Ni-TTPMA selective layer is about 210 nm ( $\pm$  3 nm). This thickness is of the same order as a layer made from a BTESE sol, having the same dip-sol concentration (260 nm [39]). The Ce-TTPMA membrane shows a very thin and homogenous selective layer of only 35 nm ( $\pm$  3 nm). The starting Ce-TTPMA sol has a bimodal particle size distribution (see Figure 5.2) with some particles smaller than pore size of the  $\gamma$ -alumina layer (5 nm). It can therefore be expected that some part of the Ce-TTPMA dip-sol penetrates inside the mesoporous  $\gamma$ -alumina layer, while another part (the bigger particles) form a smooth selective film.



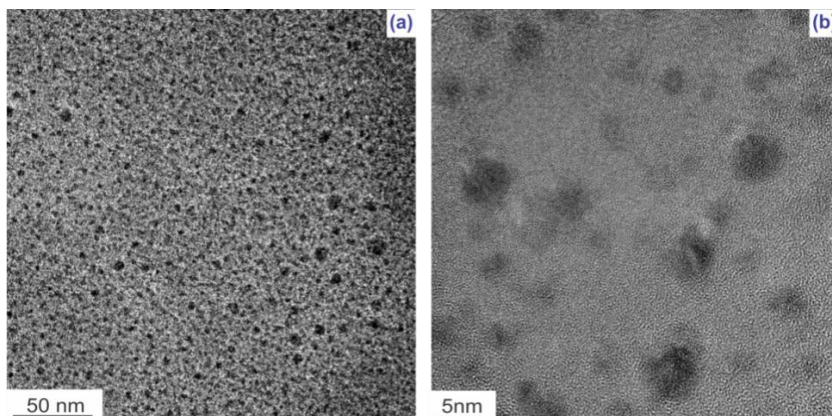
**Figure 5.3:** (a) HR-SEM images of a Ce-TTPMA membrane indicating an isotropic thin layer of about 35 nm. (b) HR-SEM images of a Ni-TTPMA membrane with an isotropic layer thickness of about 210 nm.

TEM images were made from Ce- and Ti- doped TTPMA samples to gain insight into the dispersion of ceria within the TTPMA silica matrix after calcination. In the case of Ce-TTPMA TEM data revealed the presence of small nanosized (2-5 nm) crystallites within an amorphous matrix (figure 5.4a). The crystallites, as indicated by the encircled particle (Figure 3), were found to have a lattice spacing of  $d \sim 3.1 \text{ \AA}$ . A Fourier transform image of such a crystallite is given in figure 5.4b. The observed lattice spacing value is consistent with  $\text{CeO}_2$  (111) planes [40].



**Figure 5.4:** (a) HR-TEM images of a holey copper grid (with a carbon film) dip-coated with Ce-TTPMA sol and calcined at  $T=250$  °C. (b) Fourier transform of the encircled region in section (a) of this figure.

TEM analysis on calcined Ni-doped TTPMA revealed a substantial amount of phase-separated electron rich particles. These particles with sizes ranging from 1 to 15 nm (figure 5.5) most likely consist of hydrated  $\text{Ni}_2\text{O}_3$ . As no lattice spacing could be determined for these particles, it might also be that these dark areas are clusters of “amorphous”  $\text{Ni}_2\text{O}_3$  particles in a silica (TTPMA) matrix.



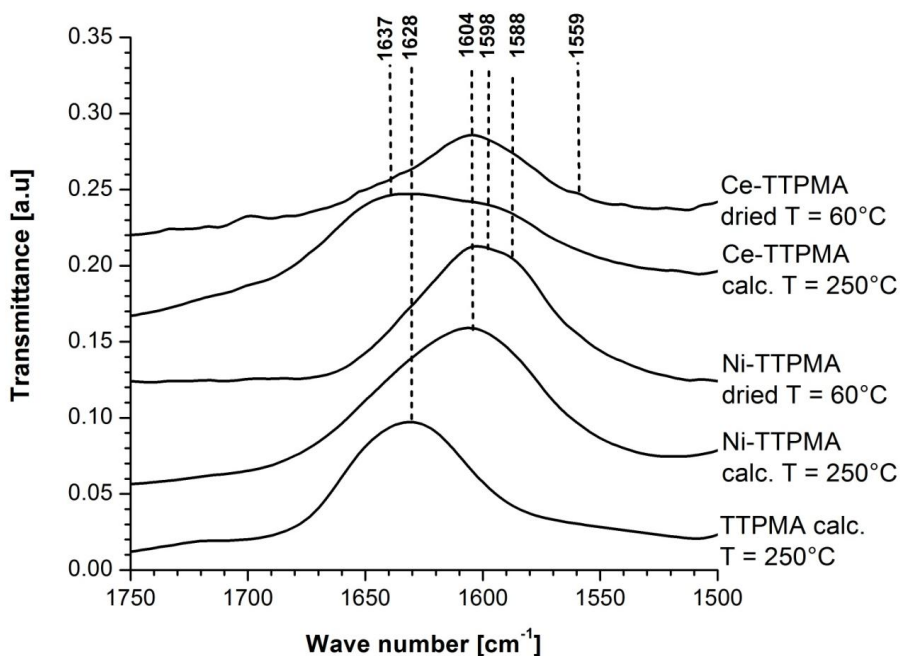
**Figure 5.5:** HR-TEM images of a copper grid dip-coated with Ni-TTPMA after calcination at  $T = 250\text{ }^{\circ}\text{C}$  at 2 different length scales. **(a)** overview image; **(b)** magnified image showing phase separated particles with sizes between 1 and 15 nm.

These TEM analyses give an indication on the metal distribution in the calcined gel. To investigate in what way the metal distribution evolves in the TTPMA matrix during calcination, FTIR analyses were performed. Figure 5.6 shows the FTIR absorbance spectra of a pure, calcined TTPMA, as well as dried and calcined gels of doped Ce-TTPMA and Ni-TTPMA.

When the Ce-TTPMA gel was dried at  $60\text{ }^{\circ}\text{C}$ , a  $\nu\text{ C=O}$  was observed with a maximum at  $\nu = 1604\text{ cm}^{-1}$ . The shoulder at  $1559\text{ cm}^{-1}$  was caused by a reduced force constant when the free C=O moiety was engaged by the metal cation [26, 41-43]. FTIR analyses reveal that the malonamide ligands are coordinated to  $\text{Ce}^{4+}$  in the dried gel, however, the exact structure could not be resolved solely by FTIR. After calcining the Ce-TTPMA sample at  $250\text{ }^{\circ}\text{C}$  for 3 hr, a new C=O vibration appeared at  $1637\text{ cm}^{-1}$ , which is very close to the  $1628\text{ cm}^{-1}$  C=O vibration of calcined TTPMA sample, which is indicative of free malonamide  $\nu\text{ C=O}$  vibrations [26, 41, 44]. Furthermore, the signal near  $1604\text{ cm}^{-1}$  decreased in intensity after calcination of the Ce-TTPMA sample, which corresponds to a reduction in the number of malonamide ligands that are coordinated to  $\text{Ce}^{4+}$ . In conclusion, cerium remains coordinated to the TTPMA ligand during sol-gel processing and drying, but during calcination at  $250\text{ }^{\circ}\text{C}$ , a substantial amount of the malonamide ligands became detached from cerium, which may subsequently have resulted in phase separation in the form of  $\text{CeO}_2$ , which also can be seen from the TEM image (figure 5.4).

When the Ni-TTPMA sol was dried at  $T=60\text{ }^{\circ}\text{C}$ , a small shoulder at  $1588\text{ cm}^{-1}$  was observed in FTIR, which can be ascribed to either nickel bounded with multiple malonamide ligands, or nickel bound with nitrate ions [45, 46]. By comparing the FTIR results of calcined TTPMA with calcined Ni-TTPMA, a clear shift in the carbonyl vibrations from  $1628\text{ cm}^{-1}$  to  $1604\text{ cm}^{-1}$  can be observed, indicating a modification in structure of TTPMA through the addition of nickel.

Further details on the FTIR results on TTPMA, Ce-TTPMA and Ni-TTPMA are given in [36].



**Figure 5.6:** FTIR-ATR absorbance spectra of pure TTPMA, Ce-TTPMA and Ni-TTPMA.

### 5.3.2 Single Gas Permeation Performance

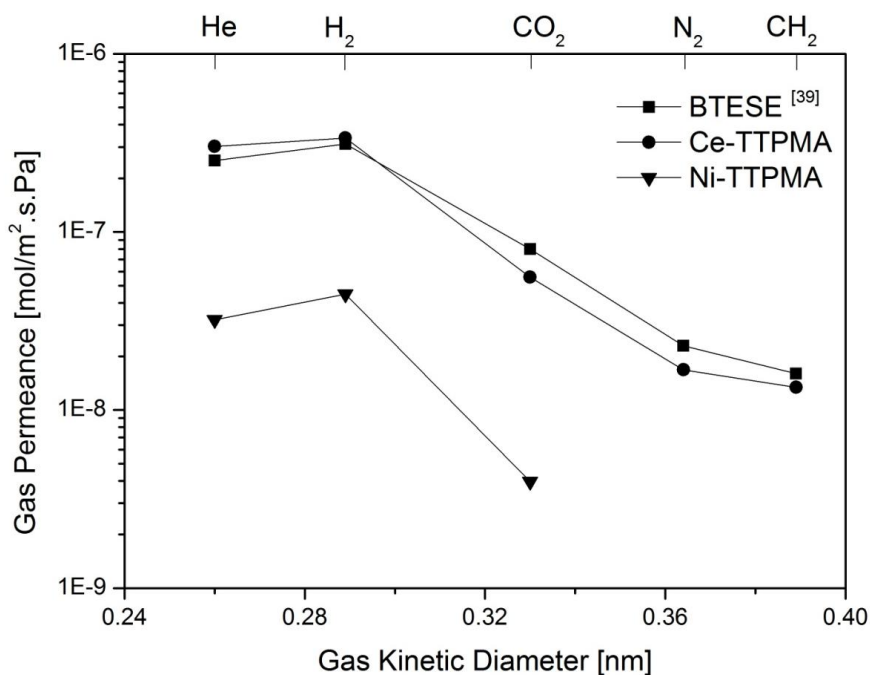
In order to obtain information on the applicability of Ce- and Ni- doped TTPMA membranes for separating small molecules ( $< 1\text{ nm}$ ), single gas permeances of individual gases ( $\text{He}$ ,  $\text{H}_2$ ,  $\text{CO}_2$ ,  $\text{N}_2$ ,  $\text{CH}_4$  and  $\text{SF}_6$ ) were performed at  $200\text{ }^{\circ}\text{C}$ . These

results are shown in figure 5.7. The permeation data are compared with membranes made from a BTESE (1,2-*bis* triethoxysilylethane) hybrid silica precursor. This BTESE membrane was calcined under identical atmosphere and heating rate, but at a higher temperature of 300 °C [39].

No permeation of hexafluoro-sulfide ( $\text{SF}_6$ ) gas was observed through either Ce-TTPMA or Ni-TTPMA membranes, indicating that the largest pore size of these membrane is less than 0.55 nm, thus a defect-free pore microstructure is established and confirmed. With Ce-TTPMA membranes, despite the affinity of cerium towards  $\text{CO}_2$ , no remarkable improvement in  $\text{CO}_2/\text{CH}_4$  permselectivity was observed as the permselectivity of 4.3 was lower than pure BTESE hybrid-silica precursor [39];  $[\text{CO}_2/\text{CH}_4]_{\text{BTESE}} = 5$ ) but was considerably higher than its corresponding Knudsen diffusion value of 0.6. Adding to that,  $\text{H}_2/\text{N}_2$  and  $\text{H}_2/\text{CH}_4$  permselectivities are not only better than their corresponding Knudsen diffusion values of 3.9 and 2.8 respectively, but also higher than a membrane made from the BTESE hybrid-silica precursor [39]. BTESE membranes showed  $\text{H}_2/\text{N}_2$  and  $\text{H}_2/\text{CH}_4$  permselectivity of 14 and 20 respectively while Ce-TTPMA membranes have  $\text{H}_2/\text{N}_2$  and  $\text{H}_2/\text{CH}_4$  permselectivities of 20 and 26 respectively (Table 5.1). These results indicate that Ce-TTPMA membranes show a slightly better permselectivity for bigger gas molecules over hydrogen than BTESE membranes and that gas transport is based on a size exclusion transport mechanism. Furthermore, a minimal variation (*i.e.* less than 5%) was observed in hydrogen permeance at the start and at the end of the gas permeation analysis, indicating that Ce-TTPMA derived membranes possessed a sustainable pore microstructure. The Ce-TTPMA membrane has a selective layer thickness of about 35 nm, while the layer thickness for a BTESE membrane was about 260 nm, using in both cases an identical dip-sol concentration. From the comparable hydrogen permeance and the thinner (seven times thinner) selective layer it can be concluded that the Ce-TTPMA membranes develop a pore microstructure with a smaller pore-size than for BTESE membranes (by assuming that permeance resistance over  $\alpha$ -alumina support and  $\gamma$ -alumina intermediate layer is identical for both membranes).

For Ni-TTPMA membranes, helium and hydrogen fluxes were one order of magnitude lower than pure hybrid silica (BTESE) membranes, with an almost identical separation layer thickness, forming a tight pore microstructure where the gas transport mechanism is dominated by molecular sieving. Nitrogen and methane

permeances were found below the detection limit of the gas permeation equipment (*i.e.* below  $5 \times 10^{-10}$  moles/m<sup>2</sup>.s.Pa), from which it can be concluded that the Ni-TTPMA membranes are nitrogen and methane impermeable at 200 °C (figure 5.7). Furthermore, the identical hydrogen permeance values observed at the start and at the end of gas permeances analysis indicated no (irreversible) structural changes in the membrane during the measurements. In [47, 48] nickel has been incorporated into a pure silica matrix in order to obtain hydrothermally stable silica membranes. However, these membranes showed some nitrogen permeance. The results reported in our work are the first results for Ni-doped silica systems that formulated nitrogen impermeable membranes.



**Figure 5.7:** Single Gas permeation results as a function of gas kinetic diameter for Ce-TTPMA and Ni-TTPMA and BTESE hybrid silica membranes.



**Table 5.1:** Single Gas Permeation and selectivity results at 200 °C of Ce-TTPMA, Ni-TTPMA and BTESE hybrid silica membranes.

Gas Kinetic Diameter [nm]	Gas Permeance ( $10^{-7}$ mol/m <sup>2</sup> .s.Pa)	Selectivity H <sub>2</sub> /X	Gas Permeance ( $10^{-7}$ mol/m <sup>2</sup> .s.Pa)	Selectivity H <sub>2</sub> /X	Gas Permeance ( $10^{-7}$ mol/m <sup>2</sup> .s.Pa)	Selectivity H <sub>2</sub> /X
<b>Ce-TTPMA (This work)</b>						
$\delta^{**} = 35$ nm						
He = 0.26	3.02	1.11	0.32	1.4	2.52	1.23
H <sub>2</sub> = 0.289	3.37	1	0.45	1	3.12	1
CO <sub>2</sub> = 0.33	0.56	6	0.04	11.3	0.8	3.9
N <sub>2</sub> = 0.364	0.17	19.8	*	$\infty$	0.23	13.5
CH <sub>4</sub> = 0.369	0.13	25.9	*	$\infty$	0.16	19.5
SF <sub>6</sub> = 0.55	*	$\infty$	*	$\infty$	*	$\infty$
<b>Ni-TTPMA (This work)</b>						
$\delta = 210$ nm						
<b>BTESE [39]</b>						
$\delta = 260$ nm						

\* Below detection limit of equipment i.e. below  $5 \times 10^{-10}$  mol/m<sup>2</sup>.s.Pa.

\*\*  $\delta$ : thickness of the separation layer.

## 5.4 Conclusions

N,N,N',N'-tetrakis-(3-(triethoxysilyl)-propyl)-malonamide (TTPMA) was synthesized successfully through a reaction of *bis*-(3-(triethoxysilyl)-propyl)-amine with malonyl chloride. The malonamide ligand of TTPMA was found to coordinate with both Ce<sup>4+</sup> and Ni<sup>2+</sup> of cerium isopropoxide and nickel nitrate hexahydrate.

For Ce-TTPMA, a CeO<sub>2</sub> phase separated while calcining the hybrid film at  $T = 250$  °C. Consequently, nanosized clusters (2-3 nm) of CeO<sub>2</sub> were formed. Single gas permeances on Ce-TTPMA membranes revealed a slightly larger H<sub>2</sub>/N<sub>2</sub> permselectivity as compared to a previously reported BTESE hybrid membrane, which was substantially thicker (260 nm) than the Ce-TTPMA layer. For Ni-TTPMA gels, after calcination, nanosized (2-15 nm) nickel oxide particles or clusters of particles were observed by TEM. The 210 nm thick selective layer of a Ni-TTPMA membrane was approximately one order of magnitude more resistive towards permeance of H<sub>2</sub>, He and CO<sub>2</sub> as compared to a hybrid BTESE layer of similar thickness. No N<sub>2</sub> permeance was observed within the experimental error for this Ni-TTPMA membrane, which makes this material a promising gas-selective material for CO<sub>2</sub>/N<sub>2</sub> separation. As future outlook, Ni-TTPMA membranes with thinner selective layer can be developed that would result in improved permeance and it would be very worthwhile to study the gas permeation properties of these membranes under hydrothermal conditions.

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## **Chapter 6**

**Mesoporous organosilica material as a  
substitute of  $\gamma$ -alumina for membrane  
applications**



## Abstract

1-2,*bis*(triethoxysilyl)octane (BTESO) was used as a precursor for the fabrication of graded ceramic membranes. Sol-gel processing showed a neat and monodispersed particle size distribution of BTESO sols with an average size of about 25 nm. N<sub>2</sub> adsorption/desorption revealed that the structure of BTESO has almost identical meso-porous properties as  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>. However, when the BTESO sol was deposited on an  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> support excessive sol infiltration occurred that inhibited the formation of a BTESO mesoporous layer onto the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> support. When the BTESO sol was deposited on a  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> support, a thin, homogenous and a crack-free layer of a few hundred nanometers was formed that offered no resistance to gas permeation at 200 °C. Strategies such as multiple dipping with or without the aid of a viscosity modifier can be employed to avoid infiltration and to improve the stability of BTESO derived thin mesoporous layers.

## 6.1 Introduction

For the fabrication of multi-layered ceramic membranes via sol-gel processing, the quality of the support is of crucial importance for the integrity of the selective layer that is applied in subsequent preparation steps [1]. A uniform pore size and porosity of the membrane support is one of the requirements for uniform deposition of an intermediate or a selective layer [2]. If properly prepared, ceramic membranes are suitable candidates in many separation applications, because of their high thermal stability, high solvent resistance (*i.e.* extreme pH or aggressive organic solvents), and ease of cleaning and long term stability [3-5].

For ceramic membranes,  $\alpha$ - $\text{Al}_2\text{O}_3$  is commonly used as a support material and  $\gamma$ - $\text{Al}_2\text{O}_3$  as a mesoporous intermediate layer [6-8]. Besides, ceramic materials like titania [9] and zirconia [10] are also used as membrane. A good starting support for making a micro porous membrane is a macroporous  $\alpha$ - $\text{Al}_2\text{O}_3$  support with a pore size in the range 70-90 nm, and a porosity of 35 % or more [11]. On such a support a few micrometer thick mesoporous  $\gamma$ - $\text{Al}_2\text{O}_3$  layer is applied with a pore size in the range of 3-5 nm and a porosity of around 50% [12]. It has been reported that macroporous  $\alpha$ - $\text{Al}_2\text{O}_3$  is chemically stable while mesoporous  $\gamma$ - $\text{Al}_2\text{O}_3$  shows poor chemical stability at low pH solutions *i.e.* pH below 3 [13, 14], which limits the use of  $\gamma$ - $\text{Al}_2\text{O}_3$  as an intermediate layer in harsh separation environments.

Microporous hybrid silica (*bis*-(triethoxysilyl)ethane [BTESE]) membranes have proven their hydrothermal and chemical stability in water removal from alcohols where these membranes are stable at a pH as low as 2 [15-17]. In this contribution, it is aimed to exploit the structural properties of another hybrid silica precursor (*bis*-(triethoxysilyl)octane [BTESO]) to assess its suitability as a substitute material of  $\gamma$ - $\text{Al}_2\text{O}_3$  as intermediate layer. BTESO possesses a flexible molecular structure with an octyl-hydrocarbon in the silica backbone and has been used in the past to develop microporous membranes for affinity based gas separation [18]. Here it is intended to develop a mesoporous structure of BTESO with the aim to fabricate an intermediate hybrid silica layer that can directly be applied on an  $\alpha$ - $\text{Al}_2\text{O}_3$  support.

## 6.2 Experimental

A  $\gamma$ - $\text{Al}_2\text{O}_3$  system was prepared from a boehmite sol as described in [2, 8]. Disc-shaped  $\gamma$ - $\text{Al}_2\text{O}_3$  membranes were prepared by dip-coating a boehmite sol with a PVA binder on  $\alpha$ - $\text{Al}_2\text{O}_3$  membrane supports (pore diameter 70-80 nm; thickness  $2.05 \pm 0.01$  mm; Pervatech, the Netherlands) followed by subsequent drying and calcination at  $650^\circ\text{C}$  as described in [2]. The boehmite-PVA dip-sol was twice coated on the  $\alpha$ - $\text{Al}_2\text{O}_3$  supports to obtain smooth intermediate layers. Dip-coating was performed in a class 100 laminar flow cupboard, situated in a class 1000 cleanroom, to minimize defect formation due to dust particles. The pore size of the  $\gamma$ - $\text{Al}_2\text{O}_3$  intermediate layer is around 3-5 nm, as measured by permporometry [19].

For the production of the hybrid silica sol, 1,2-bis(triethoxysilyl) octane (referred as BTESO; purity 97%; ABCR Germany) was used as precursor. Water was deionized at  $18.2\text{ M}\Omega/\text{cm}$  using a Millipore purification system. A polymeric sol was fabricated by drop-wise adding 2.37 ml BTESO to a nitric acid (0.31 ml; 65%; Aldrich)-water-ethanol mixture (0.39 ml water in 21.93 ml ethanol) at room temperature. This mixture was refluxed for 2 hr at  $60^\circ\text{C}$  under continuous stirring to produce a BTESO sol. The final molar ratio of BTESO sol is BTESO/EtOH / $\text{H}_2\text{O}$ / $\text{HNO}_3$  of 1/70.62/0.084/0.152.

20 ml of this hybrid sol was diluted with 20 ml of ethanol to produce a BTESO dip-sol for membrane fabrication.

The particle size of freshly prepared sols was determined by dynamic light scattering (DLS) using a Malvern Zetasizer Nano ZS at  $25^\circ\text{C}$ . Details of this method are described in previous chapters.

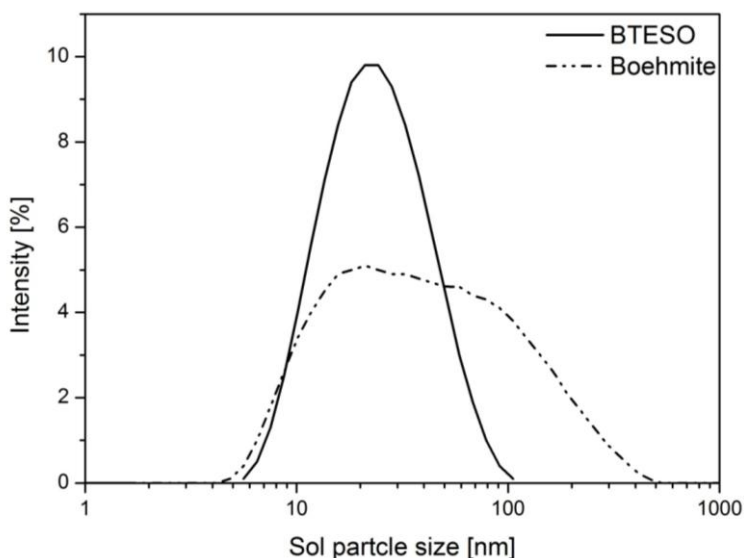
Unlike  $\gamma$ - $\text{Al}_2\text{O}_3$  layers, dip-coating of BTESO was only performed once on  $\alpha$ - $\text{Al}_2\text{O}_3$  supports. After coating of the hybrid sol, the membrane was calcined at  $250^\circ\text{C}$  for 3 hr under nitrogen flow (99.99% pure) applying a heating and cooling rate of  $1^\circ\text{C}/\text{min}$ .

The structure of calcined  $\gamma$ -alumina and BTESO gels was evaluated by nitrogen sorption porosimetry at 77K (Tristar 3000, Micromeritics). Before the measurements, the gels were degassed at  $200^\circ\text{C}$  under vacuum for 3 - 10 hrs.

Membrane characterization was performed on in-house designed single gas permeation (SGP) set-up in a dead-end mode, the details of which are also described before. The cross-sectional micrographs of developed membranes were captured by high-resolution scanning electron microscope HR-SEM (ZEISS 1550) at an accelerated voltage of 2.0 kV.

### 6.3 Results

The boehmite sol showed a broad particle size distribution ranging from about 4 to 500 nm. In contrast, the hybrid silica (BTESO) sol resulted into a neat and monodispersed size distribution ranging from about 5 nm to 100 nm with an average particle size of about 25 nm (figure 6.1).



**Figure 6.1:** Comparison of sol particle size and distribution of freshly prepared boehmite sol and BTESO hybrid sol.

Figure 6.2 shows the nitrogen adsorption/desorption results of unsupported, calcined BTESO and  $\gamma$ - $\text{Al}_2\text{O}_3$  gels. For  $\gamma$ - $\text{Al}_2\text{O}_3$ , the isotherm was a type IV-H2 hysteresis loop which was also observed previously by Uhlhorn et. al. [7]. For

BTESO, the isotherm is of type IV [20, 21] which can also be ascribed to mesoporous solids. This hysteresis can be regarded as of type IV-H4 which is associated with narrow-slit like pores [20]. The initial section (low relative pressure) of the BTESO adsorption/desorption curve is attributed to type I which is indicative for the presence of microporosity in the sample. At higher  $P/P_0$  the adsorption curve showed inclination indicative of multi-layer formation in the sample. The desorption line of the BTESO curve failed to reach zero relative pressures. During nitrogen desorption failure of the nitrogen meniscus inside the pore occurs at a relative pressure of around 0.4. If the system is not degassed properly, adsorbed nitrogen sticks to the pore walls at a relative pressure below 0.4. Therefore this part of the sorption curve does not contribute to any change in the analysis of sorption data [20, 22, 23]. In the case of BTESO, as described in this work, the desorption process did not occur completely. So, however the fact that the desorption part of hysteresis curve remained open at a partial pressure below 0.4, it is assumed that the part below 0.4 does not contribute to sorption data analysis.

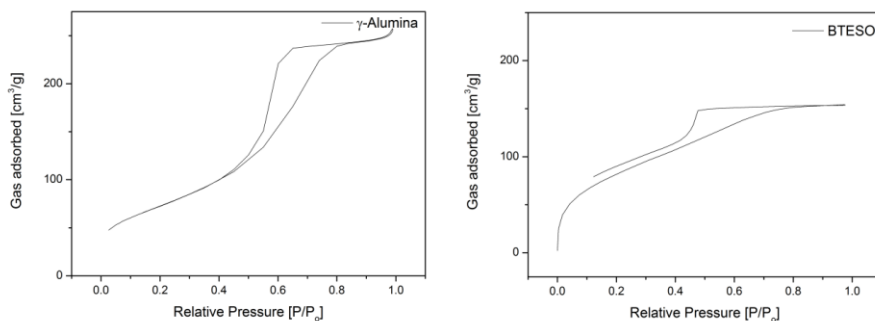
The desorption part of the  $\gamma$ - $\text{Al}_2\text{O}_3$  hysteresis starts at a higher relative pressure (almost one order of magnitude higher) than the BTESO sample. The upper limit of the pore diameter of these  $\gamma$ - $\text{Al}_2\text{O}_3$  gels is about 5 nm [24] which was later confirmed on membranes as well [19]. For BTESO, the upper limit of the pore diameter is less than 5 nm. For  $\gamma$ - $\text{Al}_2\text{O}_3$ , the relative pressure where the hysteresis loop closes is higher than for BTESO. It shows that BTESO has a lower-pore size limit than  $\gamma$ - $\text{Al}_2\text{O}_3$  (*i.e.* pore size of smallest meso pore in the sample). This could be due to presence of a large number of small mesopores or the presence of micropores. The BTESO isotherm also shows signs of microporosity at lower relative pressures.

The BET surface area of BTESO gels was calculated as  $218 \text{ g/m}^2$  and for  $\gamma$ - $\text{Al}_2\text{O}_3$  as  $240 \text{ g/m}^2$ . The mean pore-diameter of the  $\gamma$ - $\text{Al}_2\text{O}_3$  sample was 4.5 nm, which was slightly higher than what was reported previously by Leenaars and Uhlhorn, (3.5 nm) [7, 24, 25], but slightly smaller than what was recently reported by Pinheiro [26]. For BTESO, the mean pore-diameter was measured to be 3 nm (as shown in Table 6.1).

**Table 6.1:**  $N_2$ -sorption measurements of unsupported  $\gamma$ - $Al_2O_3$  and BTESO calcined gels

	<b>BET Surface area</b> [ $m^2/g$ ]	<b>Mean Pore diameter</b> [nm]
<b><math>\gamma</math>-<math>Al_2O_3</math></b>	240	4.5 nm
<b>BTESO</b>	218	3 nm

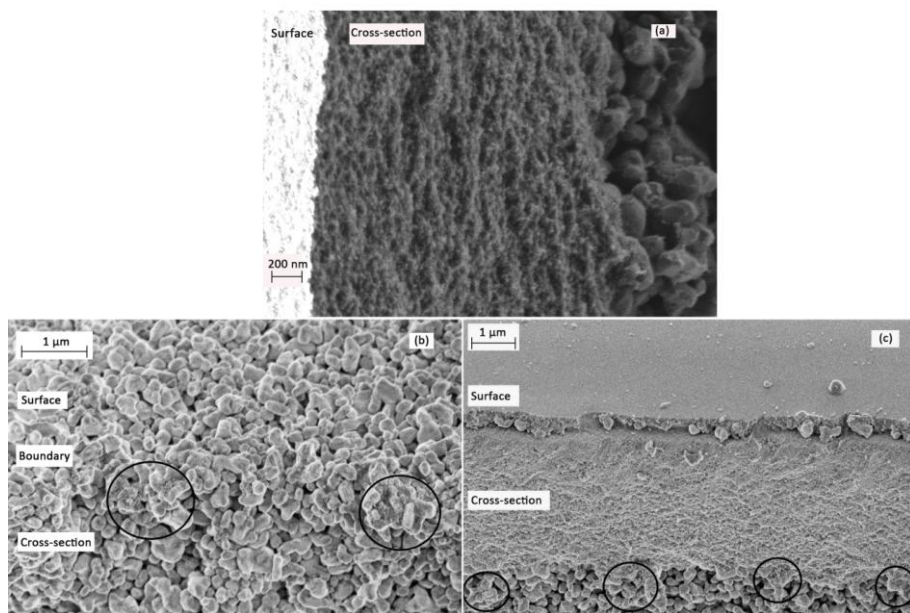
The size of the meso pores was calculated using the BJH method [20, 21]. It is reported by Uhlhorn that the pore diameter and pore structure of unsupported  $\gamma$ - $Al_2O_3$  membranes coincides with the pore size and structure of supported  $\gamma$ - $Al_2O_3$  membranes [7]. In this chapter it will now be examined, whether for BTESO it is also true that the pore morphology of calcined gels (i.e. unsupported membranes) matches with that of BTESO-supported  $\alpha$ - $Al_2O_3$  membranes and that a mesoporous BTESO layer can be applied on  $\alpha$ - $Al_2O_3$  supports by a single sol-dipping procedure, followed by a calcination step. The prepared membranes were analyzed by scanning electron microscopy and single-gas permeation tests.



**Figure 6.2:** Nitrogen adsorption-desorption isotherms of calcined BTESO and  $\gamma$ - $Al_2O_3$  gels samples.

Figure 6.3 shows high resolution SEM-micrographs of  $\gamma$ - $Al_2O_3$  and BTESO layers deposited on  $\alpha$ - $Al_2O_3$  supports. Figure 6.3(a) shows a cross-section of  $\gamma$ - $Al_2O_3$  deposited on an  $\alpha$ - $Al_2O_3$  support. Figure 6.3(b) shows an  $\alpha$ - $Al_2O_3$  support, which was dipped in a BTESO sol and subsequently calcined. In this case no separate top layer

can be observed on the  $\alpha$ - $\text{Al}_2\text{O}_3$  support. At a few places (as encircled in the figure), some small particles are visible between the  $\alpha$ - $\text{Al}_2\text{O}_3$  pores, which are expected to be BTESO particles. From this result it is concluded that the BTESO sol particles are infiltrated in the  $\alpha$ - $\text{Al}_2\text{O}_3$  support without forming a rigid layer on it. The BTESO sol, having identical mesoporosity for dried/calcined gels as for  $\gamma$ - $\text{Al}_2\text{O}_3$ , showed no indication of forming a rigid, thin layer on the  $\alpha$ - $\text{Al}_2\text{O}_3$  support. The small average particle size of BTESO could be a reason for its infiltration. To study the BTESO sol infiltration in more detail, a BTESO dip-sol was coated on a  $\gamma$ - $\text{Al}_2\text{O}_3$  support. As shown in figure 6.3 (c), a uniform BTESO layer can be observed on the  $\gamma$ - $\text{Al}_2\text{O}_3$  support. Black highlighted circles on the  $\alpha$ - $\text{Al}_2\text{O}_3$  pores indicate some BTESO sol infiltration through the  $\gamma$ - $\text{Al}_2\text{O}_3$  layer. It means that some particles of BTESO sol are even smaller than the pore size of the  $\gamma$ - $\text{Al}_2\text{O}_3$  layer. Nevertheless, the BTESO sol forms a rigid and uniform layer having thickness of about 400 nm when deposited on a  $\gamma$ - $\text{Al}_2\text{O}_3$  support by a single dipping procedure. No visible cracks on the BTESO surface are observed in the SEM-micrographs.



**Figure 6.3:** HR-SEM micrographs of supported membranes developed by using  $\gamma$ - $\text{Al}_2\text{O}_3$  and BTESO sols. **(a)**  $\gamma$ - $\text{Al}_2\text{O}_3$  deposited on an  $\alpha$ - $\text{Al}_2\text{O}_3$  membrane support. **(b)** BTESO on an  $\alpha$ - $\text{Al}_2\text{O}_3$  support. Black circles indicate BTESO sol infiltration. **(c)** BTESO on  $\gamma$ - $\text{Al}_2\text{O}_3$  /  $\alpha$ - $\text{Al}_2\text{O}_3$ .

The performance of the developed membranes was investigated by single gas permeation (figure 6.4 and table 6.2). Since it is assumed that all these membranes have pore sizes in the macro- or meso-porous range, meaning a pore diameter of 2 nm or more, gas transport will be through viscous flow or Knudsen diffusion flow [2, 3, 27, 28].

In macroporous membranes, at pore-sizes ranging 200 nm – 3000 nm, the gas transport is governed by viscous flow (often termed as Poiseuille flow) [28, 29]. In such systems, gas transport occurs under the influence of a pressure gradient across the membrane (*i.e.* pressure difference acts as a driving force) and the actual flow resistance is determined by gas viscosity ( $\eta$ ), which is why this flow is termed as viscous flow. Here, the mean free path of the gas molecule ( $\lambda$ ) is smaller than mean pore diameter, which ends up in a non-selective transport. The gas flux in such systems can be described by the Poiseuille equation which is modified by taking into account the structural geometry of the porous medium [2]:

$$N = -\frac{\varepsilon r^2}{\tau 8 \eta RT} \frac{P}{dz} \quad (1)$$

Where  $N$  is molar flux [ $\text{mole}/\text{m}^2.\text{s}$ ],  $\varepsilon$  is membrane porosity [-],  $\tau$  is the pore tortuosity [-],  $r$  is the pore radius [m],  $P$  is pressure [Pa],  $R$  is gas constant [ $\text{J}/\text{K}.\text{mol}$ ],  $T$  is absolute temperature [K].

Knudsen diffusion is typical for gas transport in systems where the pore diameter is in the range of 2 – 100 nm. Knudsen diffusion occurs when the mean free path length ( $\lambda$ ) of the gas molecule is larger than the membrane pore size. Here, the interactions between the gas molecules with each other are negligible compared to the molecule-wall interactions. Knudsen diffusion leads to gas-selectivity based on the differences in gas molecular weights. For pure Knudsen permeance, the following equation can be used.

$$F = \frac{N}{\Delta P} = -\frac{\varepsilon 2 r}{\tau 3 L} \sqrt{\frac{8}{\pi MRT}} \quad (2)$$

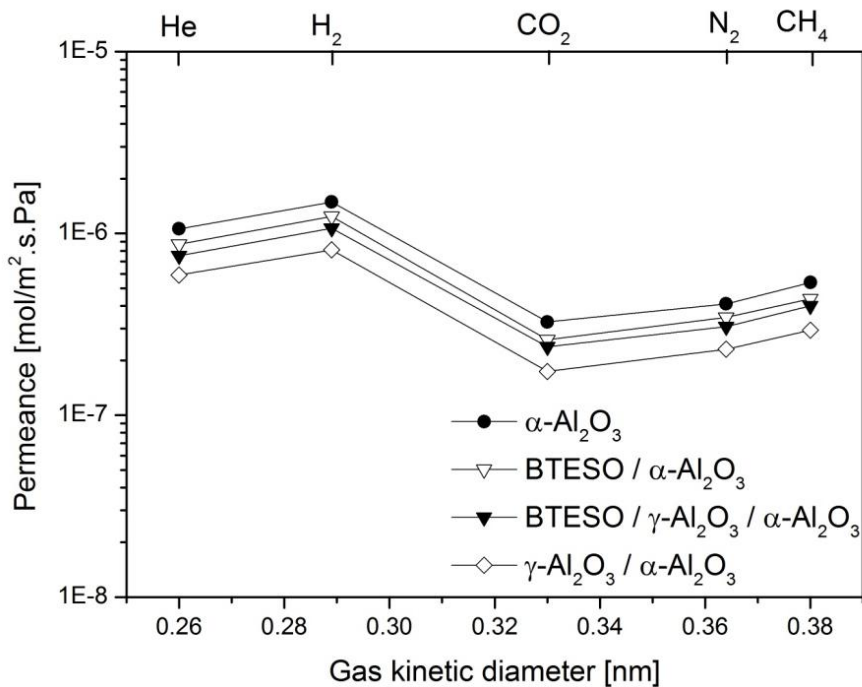
Where  $F$  is the permeance [ $\text{mol}/\text{m}^2.\text{s}.\text{Pa}$ ],  $r$  is the pore radius [m],  $L$  is membrane thickness [m], and  $M$  is the molar mass of the gas molecule [ $\text{g}/\text{mol}$ ].



For the membranes developed in this research, Knudsen diffusion transport is the dominant transport mechanism through the BTESO and  $\gamma$ - $\text{Al}_2\text{O}_3$  membranes, whereas viscous transport occurred in the  $\alpha$ - $\text{Al}_2\text{O}_3$  membranes [2, 27]. However, all the membranes show a Knudsen type of selectivity for all gases at 200 °C.

Any significant influence of applying a BTESO layer on gas transport was not observed. When BTESO was directly applied on  $\alpha$ - $\text{Al}_2\text{O}_3$ , there was a small decrease in the gas permeances which can be due to particles infiltration (as seen in figure 6.3b). When BTESO was deposited on  $\gamma$ - $\text{Al}_2\text{O}_3$ , a marginal increase in the gas permeances was observed. The variations in gas permeance were very small so there was no hard proof of BTESO influence. These small differences between the several membranes might also be due to experimental errors in the permeation measurements. So it seems that deposition of the thin BTESO on  $\gamma$ - $\text{Al}_2\text{O}_3$  has no influence on the resistance to gas flow.

Benes et. al. [29] showed on almost identical membranes that the resistance to gas flow was negligible over the relative thin (few  $\mu\text{m}$  thick)  $\gamma$ - $\text{Al}_2\text{O}_3$  layer and that the main resistance to permeation comes from the  $\alpha$ - $\text{Al}_2\text{O}_3$  support which has a thickness of around 2 mm. The BTESO layer is almost 6-7 times thinner than the  $\gamma$ - $\text{Al}_2\text{O}_3$  and gas permeation results show that this layer also offers no extra resistance to permeance at 200 °C.



**Figure 6.4:** Single gas permeation (SGP) analysis of BTESO,  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> membranes at 200 °C.

**Table 6.2:** Single gas permeation (SGP) analysis of BTESO,  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> membranes at 200 °C. Knudsen selectivity is indicated in between brackets.

	Gas Permeances [mol/m <sup>2</sup> .s.Pa]					Permselectivity			
	He	H <sub>2</sub>	CO <sub>2</sub>	N <sub>2</sub>	CH <sub>4</sub>	H <sub>2</sub> /He (1.4)	H <sub>2</sub> /CO <sub>2</sub> (4.7)	H <sub>2</sub> /N <sub>2</sub> (3.7)	H <sub>2</sub> /CH <sub>4</sub> (2.8)
$\alpha$ -Al <sub>2</sub> O <sub>3</sub>	1.06E-6	1.49E-6	3.26E-7	4.1E-7	5.38E-7	1.4	4.5	3.6	2.8
$\gamma$ -Al <sub>2</sub> O <sub>3</sub>	5.91E-7	8.12E-7	1.74E-7	2.31E-7	2.94E-7	1.4	4.6	3.5	2.7
BTESO/ $\gamma$ -/ $\alpha$ -Al <sub>2</sub> O <sub>3</sub>	8.71E-7	1.24E-6	2.6E-07	3.45E-7	4.37E-7	1.4	4.7	3.6	2.8
BTESO / $\alpha$ -Al <sub>2</sub> O <sub>3</sub>	7.55E-7	1.07E-6	2.38E-7	3.07E-7	4E-7	1.4	4.5	3.5	2.6

Detection limit of equipment: 5 X 10<sup>-10</sup> mol/m<sup>2</sup>.s.Pa.

## 6.4 Discussion

The average particle size of the BTESO sol is 25 nm and that of the boehmite sol is about 45 nm, with high polydispersity. From figure 6.1, it is clear that the proportion of small sol particles (for example,  $< 30$  nm) in the boehmite sol is considerably less compared to that of the BTESO sol. Due to this reason, the large amount of small BTESO particles can easily penetrate in the  $\alpha$ - $\text{Al}_2\text{O}_3$  support during the dip-coating procedure, while for the boehmite sol a layer is formed by the relative large amount of particles which have a size equal or larger than the pore size of the  $\alpha$ - $\text{Al}_2\text{O}_3$  support. So a bigger average particle size of BTESO is important for not penetrating in the  $\alpha$ - $\text{Al}_2\text{O}_3$  support. The particle size of BTESO sols can be increased by either increasing its concentration during sol synthesis or by prolonging the synthesis time. However, care must be taken to avoid gelation during the condensation reaction, as concentrated sols tend to gelate quickly [30].

In order to avoid BTESO sol infiltration in the  $\alpha$ - $\text{Al}_2\text{O}_3$  supports other strategies, than starting with bigger sol particles, can be applied as well. The use of a binder during sol-synthesis or in the dip-sol can be a suitable strategy. For example, Uhlhorn et al. [7] added a binder (PVA solution) to the boehmite dip-sol and performed multiple dipping (*i.e.* 2x) that resulted in the formation of a defect-free  $\gamma$ - $\text{Al}_2\text{O}_3$  layer on an  $\alpha$ - $\text{Al}_2\text{O}_3$  support. Boffa et al. [32] used a surfactant (cetyl-trimethyl-ammonium bromide CTAB) during the synthesis of silica sols and used a rheological additive (BYK-420) in small proportions (2-6 vol %) in the dip-sol to avoid sol infiltration. BYK-420 is a modified urea solution that is used in aqueous coatings as anti-settling agent for pigments [33]. Besides, in the work of Boffa et al. the silica dip-sol was coated twice on the  $\alpha$ - $\text{Al}_2\text{O}_3$  membrane supports.

It is shown that after calcination at 250 °C a mesoporous BTESO structure can be obtained by gelation of a 25 nm BTESO sol. A uniform BTESO layer was formed on an already established meso-porous  $\gamma$ - $\text{Al}_2\text{O}_3$  layer. It elucidates that particle size of BTESO sols was adequate to form a rigid mesoporous BTESO layer on a  $\gamma$ - $\text{Al}_2\text{O}_3$  support.

It must also be emphasized that layer formation is a distinct and separate phenomenon that is dependent on several structural properties of a material. The

surface area, porosity, and pore size, as measured on dried/calcined gels is not in all cases a direct proof that a rigid coating with the same microstructure will be formed after dipping the sol on a (macro) porous support and subsequent calcination. Thin layer deposition is an entire different phenomenon that involves complex kinetics like substrate wettability, contact time, drying, calcination, environment and duration of drying and calcination etc. as have been extensively discussed by Bonekamp [31].

As an outlook for further research, it is recommended to focus on increasing the particle size of BTESO hybrid sols. Multiple dipping with sol particle size of about 40-50 nm, and the use of viscosity modifiers like BYK-420 in the BTESO dip-sol would most likely result in the sustained deposition of a BTESO layer on an  $\alpha$ - $\text{Al}_2\text{O}_3$  membrane support.

## 6.5 Conclusions

Hybrid silica (BTESO) sols were successfully synthesized with an average particle size of about 25 nm. When this sol was deposited on an  $\alpha$ - $\text{Al}_2\text{O}_3$  macroporous support via dip-coating, it was not possible to form a smooth layer as was observed for  $\gamma$ - $\text{Al}_2\text{O}_3$ . When the BTESO sol was deposited on a  $\gamma$ - $\text{Al}_2\text{O}_3$  support, a uniform layer was formed and showed no additional resistance to gas transport through the membrane. The membranes showed permselectivities in the Knudsen selectivity range. To develop a smooth BTESO layer on an  $\alpha$ - $\text{Al}_2\text{O}_3$  support, it is recommended to increase the sol particle size of BTESO sols up to at least 40 nm and to use a sol viscosity modifier (for e.g. BKY-420) that would prevent sol infiltration and could lead to stable deposition of BTESO on  $\alpha$ - $\text{Al}_2\text{O}_3$  membrane supports. Finally it is advised to use multiple dipping to have sustained deposition of BTESO on  $\alpha$ - $\text{Al}_2\text{O}_3$ .

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## **Chapter 7**

### **Conclusions and Recommendations**

## 7.1 Conclusions and Evaluation

In this thesis the fabrication and viability of hybrid silica (*i.e.* BTESE) membranes for molecular separation is described. The focus is on gaining a better insight in the membrane fabrication process of these organosilica membranes and to further broaden their application range.

In the past decades, ceramic membranes prepared by sol-gel methods have been investigated for molecular separation applications. Especially silica membranes were studied in great depth [1-3]. These silica membranes have intrinsic limitations with regard to hydrothermal stability [4, 5]. This has paved the way for hybrid silica (BTESE) membranes which possess high hydrothermal stability, even under acid environments, and show good performances in pervaporation for dewatering of several alcohols [6, 7]. With regard to applications, the main objective of this work is to obtain a good performance in gas separation for these membranes as well. This is tried to be achieved via a better understanding of the pore formation mechanism during gelation while dip-coating and subsequent drying and calcining. In this way it might be possible to *orchestrate* the pore structure in a better and more controlled way.

In **Chapter 2**, a one-pot, facile and reproducible acid-catalyzed sol synthesis for the fabrication of hybrid silica membranes is described. The resulting membranes show a uniform membrane pore-microstructure with pore sizes  $< 1$  nm and gas permselectivities based on molecular sieving. Several attempts are described in literature to prepare membranes by sol-gel processing from the same precursor (*i.e.* BTESE). In almost all these cases fabrication steps are found to be tedious (more reaction steps) and more time consuming (6-8 hrs processing) if compared with the method given in chapter 2. Besides, a less uniform pore size distribution with bigger pores is reported in literature [8, 9].

In this chapter reaction parameters (precursor concentration [Si], acid ratio [AR =  $H^+$  : Si], hydrolysis ratio [HR =  $H_2O$  :  $OC_2H_5$ ]) and processing conditions (temperature, time) are well described and their influences on sol, (dried and calcined) gel and membrane properties are explained. It is stressed that making the optimal hybrid silica sol for a membrane demands a defined precursor concentration, an optimized

hydrolysis and condensation reaction as well as a reaction time and temperature that results in stable, non-gelated and uniform sols with average particle sizes ranging from 7-10 nm. It was figured out that by tuning the precursor concentration ( $[\text{Si}] = 1.8 \text{ M}$ ), hydrolysis ratio ( $\text{HR} = 1$ ), acid ratio ( $\text{AR} = 0.1$ ) and reaction time and temperature ( $60 \text{ }^\circ\text{C}$  and 90 minutes), the sol synthesis resulted in a hybrid silica sol, applicable for membrane fabrication. After proper dilution of the sol it was possible to make thin selective layers on a porous support after coating of the “dip-sol” and subsequent calcining. A direct relation between dip-sol concentration, resulting selective layer thickness and gas permselectivities was observed. With an increase in dip-sol concentration the membranes showed a higher  $\text{H}_2/\text{CH}_4$  selectivity. Dip-sol concentrations higher than 0.6 M resulted in cracked membranes with crack-lines visible by the naked-eye (as shown in figure 2.3). On the other hand, reduced dip-sol concentrations resulted in ultrathin selective layers with thicknesses less than 100 nm and increased permeances of larger molecules ( $\text{N}_2$ ,  $\text{CH}_4$ ) but still impermeable to  $\text{SF}_6$ . Based on gas transport theory and permeance data, a relatively concise estimation of the pore size range of the developed BTESE membranes is reported. It was shown that these hybrid silica membranes possess a pore size ranging from 0.3 to 0.54 nm.  $\text{SF}_6$  impermeable BTESE membranes are made, which, to the best of our knowledge, has never been reported before. To summarize, it was shown that the pore-size of BTESE membranes can be adjusted to some extent by tuning the dip-sol concentration.

The knowledge, acquired in chapter 2, regarding the control of sol processing and membrane fabrication, is used for further research as described in **Chapter 3**. The aim was to induce changes in the sol fabrication process to modify the BTESE membrane microstructure in such a way that it can be targeted for the separation of small gas molecules ( $< 0.4 \text{ nm}$ ). In chapter 3 the effect of adapting the acid concentration during the sol synthesis on the BTESE membrane microstructure is discussed. Ten times less acid was used to prepare BTESE sols, while the sol polymerization time was reduced to 30 minutes. Microporous membranes, prepared in this way showed a more tight pore-microstructure than was found from the results as described in chapter 2.

It was observed in chapter 2 that hydrolysis ratios above 1 and acid-ratios above 0.1 (including all possible combinations) resulted in a gelated sol structure even after

reaction at ambient (room) temperature. In chapter 3, along with reducing the acid ratio from 0.1 to 0.01, the precursor concentration was increased from 1.8 M to 2.7 M to achieve a sufficient large sol particle size under these relative acid lean conditions. The higher pH of this sol system (compared to the pH applied in chapter 2) leads to a slower hydrolysis reaction which resulted in a more controlled and homogeneous growth of sol particles without fast gelation [10, 11]. In this way the non-gelation boundaries of hybrid silica sol processing were extended by combining a reduced acid ratio (AR = 0.01) with a high Si precursor concentration (2.7 M) and a hydrolysis ratio of 1. Here the best result in terms of membrane characteristics was obtained after reaction for 90 minutes at 60 °C. The reproducible results on sols and membranes showed that, with a high dip-sol concentration of 0.6 M, a uniform selective hybrid silica layer of 440 nm was formed that showed a H<sub>2</sub>/N<sub>2</sub> permselectivity of at least 50. At some instances these membranes were also found nitrogen and methane impermeable.

Membranes developed from sols prepared in a water lean condition, meaning a hydrolysis ratio (HR) of 0.5, (acid ratio: 0.1) showed very high gas permeances and low H<sub>2</sub>-permselectivities (H<sub>2</sub>/N<sub>2</sub> = 5; H<sub>2</sub>/CH<sub>4</sub> = 4; H<sub>2</sub>/SF<sub>6</sub> = 300). This could be due to insufficient formation or presence of siloxane bonds in the selective layer after calcination. Sol growth under water lean conditions can result in non-gelated sols with particle sizes adequate to form membranes, but care must be taken to add sufficient water during sol synthesis for silanol (and siloxane) formation [11]. In the studied system, we can say that probably not all the BTESE was hydrolyzed under the HR of 0.5.

In literature it was concluded from experimental [12, 13] and molecular simulation research [14, 15] that the permselectivity for hybrid silica membranes can be tuned by tuning the length of the organic functional groups between the silica moieties. With these “spacer techniques”, *i.e.* adjusting the length of the hydrocarbon bridge, the membrane pore size can be altered. This also demands adaptations in the sol synthesis route for each precursor. In chapter 3 a new approach is presented, which shows that pore structure tuning of the hybrid silica matrix can also be performed by modifying the reaction parameters of a specific precursor during sol synthesis. Based on the ease-of-use in membrane development and the overall high

membrane performances, the strategy mentioned in this chapter clearly prevails over previous claims of structural tuning by spacer technology.

**Chapter 4** presents a new approach to incorporate different elements in the BTESE matrix by acid catalyzed sol processing. After doping BTESE with other ions a well-defined sol particle size and particle size distribution as well as the tendency to gelate (and consolidate) without cracking during dip-coating and calcination is imperative in forming a uniform membrane microstructure. For example, Nb-doping in a silica matrix has resulted in improved hydrothermal stability of silica membranes [16], which was mainly due to the fact that the doped element was coherently dispersed in the silica structure and improved its stability without damaging the structure of the selective layer.

Boron, niobium, and tantalum were doped in the BTESE matrix with the aim to enhance the gas permselectivities. An in-situ FTIR analysis was conducted to ensure successful incorporation of these elements in the BTESE matrix. TGA and FTIR results on all dried and calcined doped-BTESE gels ensured that the ethylene bridge in doped-BTESE was retained in inert gas atmosphere until at least 500 °C. The developed membranes tend to form a relatively loose microstructure than undoped BTESE membranes as indicated by higher single gas permeances. High resolution scanning electron microscopy studies showed no visible defects or cracks in the membrane layers *i.e.* all doped-BTESE materials formed a smooth and uniform selective layer. As the dopant and dip-sol concentrations were identical for all doped membranes, any difference in the selective layer thickness must be ascribed to the effect of the presence of the specific doping element on the selective layer microstructure. The Ta-BTESE layer thickness (230 nm) was relatively close to the layer thickness of pure BTESE (260 nm), but a large decrease in H<sub>2</sub>/N<sub>2</sub> and H<sub>2</sub>/CH<sub>4</sub> permselectivities was observed. The B-BTESE (180 nm) layer thickness was found to be much thinner than that of undoped BTESE and an excessive permeance was observed for bigger gas molecules such as N<sub>2</sub>, CH<sub>4</sub> and even SF<sub>6</sub>, indicating the formation of a very open/loose pore network for these B-BTESE membranes. On the other hand, the Nb-BTESE selective layer was 360 nm thick which is almost 40% thicker than undoped BTESE, while nitrogen and methane permeances were found respectively 80% and 60% higher than undoped-BTESE membranes with reduced the H<sub>2</sub>/N<sub>2</sub> and H<sub>2</sub>/CH<sub>4</sub> permselectivities. The fabrication strategy presented in this

work resulted in doped-BTESE sols, adaptable for membrane coating, but the prepared membranes were found to have a lower permselectivity compared to undoped BTESE membranes. These results show that sol synthesis and membrane fabrication are two distinct and independent phenomena and a “good” hybrid sol does not necessarily guarantee a good a membrane. Furthermore, with Nb-BTESE, no clear affinitive effect towards CO<sub>2</sub> permeance was observed contrary to what was reported earlier by Qi et. al. [17].

In **Chapter 5** an approach to disperse metal-ions in a new type of hybrid silica precursor, named *N,N,N',N'*-tetrakis-(3-(triethoxysilyl)-propyl)-malonamide (TTPMA), is described. This precursor was synthesized by a base-catalyzed nucleophilic substitution of bis-(3-triethoxysilyl)-propyl)-amine on malonyl chloride. Ce and Ni ions were introduced in the malonamide ligand, and from the developed sols membranes were fabricated and characterized. TEM observations on calcined samples showed that nano-particles of cerium oxide (2-4 nm) and nickel oxide (2-15 nm) were present in the Ce-TTPMA and Ni-TTPMA membranes respectively. The sol particle size distribution was bimodal for Ce-TTPMA sols (figure 5.2), while a smooth and ultra-thin selective layer of 35 nm was formed that showed slightly better H<sub>2</sub>/N<sub>2</sub> and H<sub>2</sub>/CH<sub>4</sub> permselectivity than BTESE membranes. Ni-TTPMA formed well-defined sol particles that resulted in membranes with a selective layer thickness of 210 nm (*i.e.* 20% thinner than that of BTESE). The gas fluxes of smaller gases (*i.e.* He, H<sub>2</sub>) through these membranes were one order of magnitude lower than BTESE membranes with no detectable permeation of nitrogen or methane, showing that the Ni-TTPMA pore network was too dense to allow any permeation of nitrogen or methane.

As a future outlook, it would be worthwhile to perform hydrothermal stability and chemical resistance tests on these membranes. Furthermore, doping of metals such as Nb, and Ta in a TTPMA membrane matrix should be conducted to enable direct comparison with Ta and Nb doped BTESE membranes.

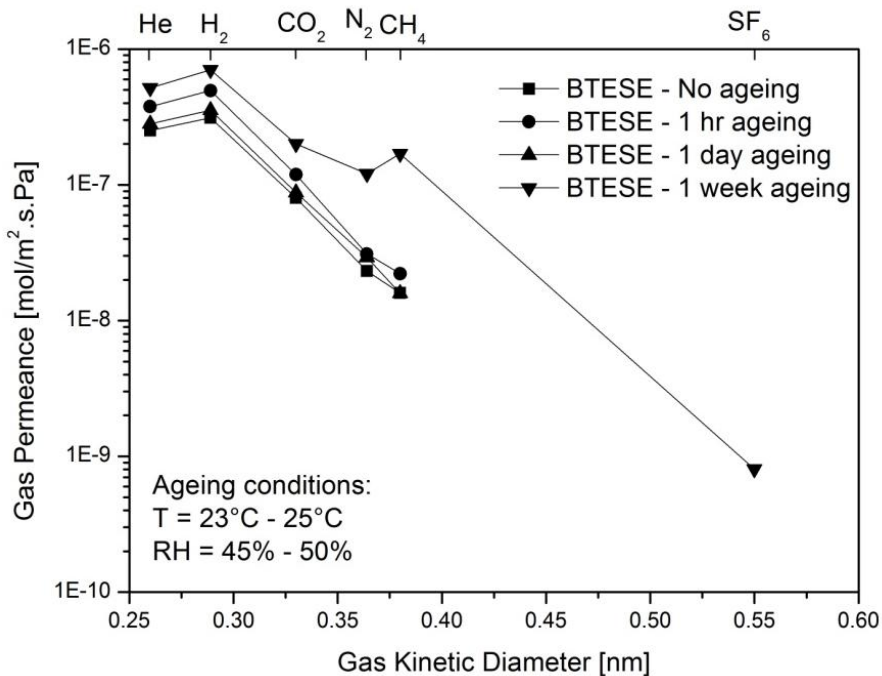
In literature another way to reduce the pore size of silica membranes is described. This so-called “ageing” implies that after dipping the freshly prepared silica membranes were left in a controlled environment (temperature and humidity) for a certain period of time, prior to calcination [18]. BTESE membranes were developed as stated in chapter 2, and were aged at different time intervals to study the effect

of ageing on the BTESE pore microstructure. As can be seen in table 7.1 and figure 7.1, there was a marginal improvement in  $H_2/N_2$  and  $H_2/CH_4$  permselectivities when the BTESE membranes were aged for 1 hr after dip-coating prior to membrane calcination. Prolonged duration of membrane ageing (*i.e.* 1 week to 3 weeks) resulted in a drastic reduction of  $H_2$ -permselectivities which were found closer to Knudsen selectivities. So, in our work we did not observe any improvement in (perm) selectivity by “ageing” the dip-coated membranes prior to calcining. It could be that when left in air for long time intervals after dipping, the siloxane gel was infiltrated in the underneath support.

**Table 7.1:** Permselectivity data of BTESE membranes recorded at 200 °C, when aged for different intervals after dip-coating and before calcination.

Permselectivity ( $H_2/X$ )	BTESE (300)				
	(No ageing)	(1 hr)	(1 day)	(1 week)	(3 weeks)
$H_2/He$	1.2	1.3	1.2	1.3	1.4
$H_2/CO_2$	3.9	4.1	4.0	3.5	4.5
$H_2/N_2$	13.5	16	12	6	3.7
$H_2/CH_4$	19.5	22.2	22.3	4.1	4.1
$H_2/SF_6$	$\infty$	$\infty$	$\infty$	875	850
$CO_2/CH_4$	5	5.5	5.5	1.1	1.1



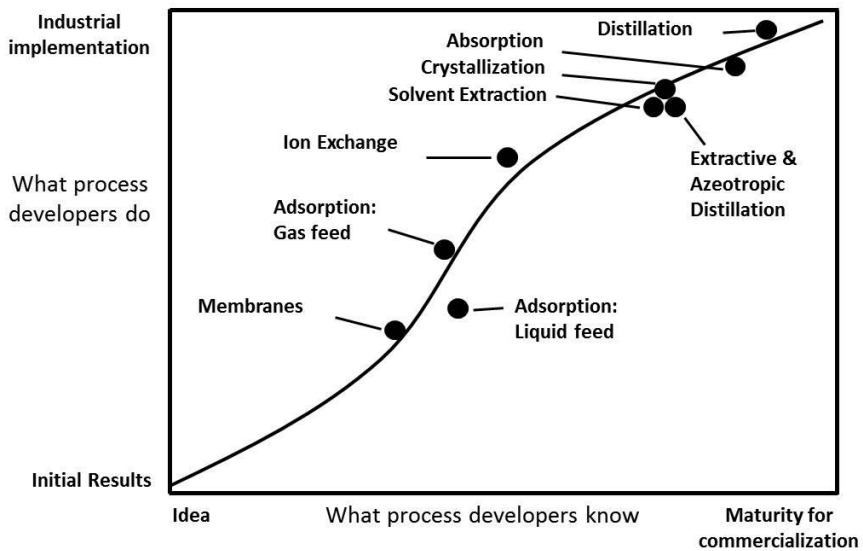


**Figure 7.1:** Single gas permeation analysis of BTESE membranes at 200 °C after ageing for different durations before subsequent calcination.

**Chapter 6** describes the fabrication and characterization of another hybrid silica material 1,2-bis(triethoxysilyl) octane (BTESO) for its applicability as a substitute material for mesoporous  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> membrane layers. Hybrid silica mesoporous interlayers would extend the applications of membranes in processes where hydrothermal and chemical stabilities are of paramount importance. BTESO sol synthesis resulted in sols with average particle sizes of about 25 nm and a neat size distribution, whereas the dried and calcined gel formed into a mesoporous structure. However, when the sol was deposited on an  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> support by dip-coating, the particles penetrated in the support without forming a rigid surface layer. This was probably due to the small average particle size of BTESO sols in relation to the pore size of the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> support (80 nm). It is assessed that an increase in the BTESO sol particle size up to at least 40 nm would reduce its infiltration effects considerably.

## 7.2 Recommendations

Figure 7.2 [19] shows the exploitation trends for various separation processes based on their fundamental understanding and commercial implementation. The x-axis of this figure represents the growth trend of an invention from an idea towards its maturity for entering in the market. The y-axis shows the growth trend of a process from initial results to its fully utilization.



**Figure 7.2:** Technological and use maturities of separation processes [19].

As can be seen from this figure, a process such as distillation is fully understood and is commercially utilized for its benefits in purification and separation domains. On the other hand, membranes still have a lot to offer with regard to their fundamental understanding and commercial viability. Due to their ease-of fabrication and energy-efficient performance with no waste generation, membranes can be seen as one of the most viable separation tool to serve humanity in the future surrounding with scarce energy resources and less-clean environment. However, for sol-gel derived membranes a better understanding of precursor chemistry, a better control of reaction kinetics and microstructure development is still necessary for fully

translating these types of membranes into applications, ranging from microfiltration to molecular separation.

The hybrid silica membranes, as described in this thesis, certainly have a place in future separation processes. Orchestrating their pore microstructure, either by tuning the synthesis parameters or by addition of dopants, would certainly enhance their viability in applications ranging from gas separation ( $d_p < 0.4$  nm) to nanofiltration ( $d_p > 1$  nm). The membranes, described in chapter 3, showed excellent  $H_2/CH_4$  and  $CO_2/CH_4$  permselectivities. The next step could be to utilize their applicability in biogas purification / upgrading. The polymeric membranes (such as cellulose acetate) currently in use for this process show poor  $H_2S$  stability and they plasticize at high  $CO_2$  partial pressure [20]. BTESE membranes are less prone to attack by  $H_2S$  and don't plasticize in  $CO_2$  and therefore these membranes are promising to be applied in biogas upgrading.

In chapter 6, BTESO was synthesized and it formed a mesoporous structure. Orchestrating the fabrication strategy of BTESO to develop micro/meso porous membranes would result in membranes with bigger pores than BTESE and a more hydrophobic surface due to the presence of an increased number of hydrocarbon chains. The water contact angle of BTESE membranes developed in chapter 2 was  $64^\circ \pm 2$ , with BTESO membranes it is expected to be above  $85^\circ$ . The larger pore size and the more hydrophobic character of BTESO-derived membranes could yield interesting nanofiltration membranes for energy effective recovery of solvents from waste chemical streams. Solvents such as alcohols, THF, acetonitrile could be recovered in an effective way either by using these membranes or by coupling the developed membranes with distillation columns, thus making a hybrid separation process. The increased hydrophobicity can also be utilized in dehydration of natural gas.

Tuning the reaction parameters of BTESO for obtaining bigger sol particles as achieved in chapter 6 would cease sol entrainment in the underneath  $\alpha-Al_2O_3$  support layer. In this way a graded BTESE / BTESO /  $\alpha-Al_2O_3$  membrane could be fabricated that can be used in separation processes at very low pH ( $< 2$ ) where it was not used before due to decomposition of the  $\gamma-Al_2O_3$  layer.

Tuning of the pore size of BTESE membranes can also be achieved by incorporating small organic monomers to its matrix during sol synthesis. A thermal treatment of the resulting “templated” membrane layer would end-up in burning-off the monomer from the BTESE matrix, resulting in creating cavities having the size of the burnt monomer. However, care must be taken in the choice of monomers that can burnt off completely below 200 °C in air or below 400 °C in inert atmosphere without leaving any residue.

Ni-TTPMA derived membranes showed a N<sub>2</sub>-impermeable microstructure but the low permeances of helium and hydrogen indicated a very tight pore structure. Tuning of reaction parameters or reducing the dipping concentration of Ni-TTPMA sols could result in a thinner selective layer to obtain larger fluxes for small gases like He and H<sub>2</sub>.

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# Summary



This thesis deals with the synthesis and applicability of sol-gel derived porous hybrid silica membranes and their feasibility in molecular separation applications. A special emphasis was given to process parameters, which are found responsible for *orchestrating* the pore structure of the microporous membranes.

**Chapter 1** gives a brief overview of acid catalyzed sol-gel derived silica membranes which have been used for molecular separations. These membranes show an exceptional high selectivity under dry conditions but their performance under hydrothermal conditions was found to be low due to their insufficient inherent stability against steam. Two different strategies are reported in literature to deal with this issue; either by the addition of metal ions in the silica matrix, or by incorporating hydrocarbons (either as a bridge or at terminals) in the silica matrix. Both routes have resulted in the improved hydrothermal stability of silica system. The possibility of utilizing bridged-hydrocarbons in silica system *i.e.* hybrid silica, has not been studied in details for gas separation, which was one of the aims of this research.

**Chapter 2** describes the fabrication of hybrid silica membranes that were reproducibly prepared from a single-step sol-gel synthesis route, using an ethoxy-bridged silane (1,2-bis(triethoxysilyl)ethane: BTESE) as precursor. The resulting membrane, obtained by a single dipping/calcining step, had a relative more open micropore structure than pure silica membranes. The sol process parameters such as precursor concentration, acid ratio and hydrolysis ratio were tuned to develop a mono-modal particle size distribution. The H<sub>2</sub>-permselectivity, obtained at 200 °C, and thickness of the selective hybrid layer was found to be dependent on the dip-sol concentration. The developed membrane microstructure was found defect-free and SF<sub>6</sub> impermeable whereas, the selective layer thickness ranging from 90 nm to 500 nm were obtained at dip-sol concentrations of 0.15 M and 0.6 M respectively.

**Chapter 3** exploits the understanding of BTESE membranes fabrication as explained in chapter 2, to produce membranes that showed improved permselective properties. Here a more efficient and effective procedure was presented to synthesize a hybrid silica (BTESE) sols. By reducing the acid concentration with a factor 15, compared to the sol synthesis as described in chapter 2, BTESE sols were synthesized at a much faster rate *i.e.* at a condensation time of 30 minutes, resulting in homogenous hybrid sols that formed a more constricted pore

microstructure to what was observed in chapter 2. The developed membranes showed sufficient hydrogen permeance but were found almost nitrogen and methane impermeable at 200 °C ( $H_2/N_2$  permselectivity more than 50 and for  $H_2/CH_4$  90 or more). A defect-free microstructure was obtained with a selective layer thickness of about 440 nm at a dip-sol concentration of 0.6 M.

**Chapter 4** reported the doping effect of elements in the BTESE membrane matrix. A new approach of doping boron, niobium or tantalum in BTESE by sol-gel processing was introduced and microporous membranes were fabricated by a single dipping procedure. TGA studies on dried samples and FT-IR analysis on calcined samples confirmed the presence of an ethylene-bridge between the Si atoms in all metal-doped BTESE samples and the material was found thermally stable until at least 500 °C in inert atmosphere. Although the single gas permeation results indicated a relatively open pore microstructure for all doped BTESE membranes when compared with undoped-BTESE membranes, the HR-SEM showed no defects or cracking in or in the selective microporous selective layer.

To facilitate the homogenous dispersion of metal-ions in a hybrid silica matrix, a new type of hybrid silica precursor named *N, N, N', N'*-tetrakis-(3-ethoxysilyl)-propyl)-malonamide (TTPMA) is studied in **chapter 5**. TTPMA was synthesized under base-catalyzed conditions and Ce and Ni ions were introduced in the malonamide ligand to fabricate microporous membranes. TEM-results showed cerium oxide nanoparticles (2-4 nm) and nickel oxide nanoparticles (2-15 nm) in the calcined Ce-TTPMA and Ni-TTPMA samples. HR-SEM micrographs showed that both Ce-TTPMA and Ni-TTPMA membranes formed a defect-free microstructure. Ce-TTPMA membranes formed an ultra-thin selective layer of about 35 nm that showed slightly better  $H_2/N_2$  and  $H_2/CH_4$  permselectivity at 200 °C than BTESE membranes. Ni-TTPMA membranes formed a selective layer of about 210 nm and showed one order of magnitude lower gas flux of the smaller gases (*i.e.* He,  $H_2$ ) if compared with BTESE membranes, while no detectable permeation of  $N_2$  or  $CH_4$  was observed, indicating a more dense pore network than BTESE membranes.

**Chapter 6** presented the fabrication and characterization of the hybrid silica material 1,2-*bis*(triethoxysilyl) octane (BTESO) as a possible alternative material for mesoporous  $\gamma$ - $Al_2O_3$  membrane interlayers.  $\gamma$ - $Al_2O_3$  membranes have a limited stability under extreme pH and hydrothermal conditions. Replacement by BTESO

would extend application of these membranes in environments where chemical and hydrothermal stability is of paramount importance. BTESO sols with an average particle size of about 25 nm were synthesized by acid catalyzed sol processing and its calcined gels showed a mesoporous microstructure. When coated on  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> supports, BTESO sol penetrated in the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> support without forming a smooth and rigid layer. The penetration of the BTESO sol particles was probably due to the small average particle size of BTESO sols compared to the average pore size of the  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> support (about 80 nm). Increasing the average particle size of BTESO sols up to at least 40 nm would significantly reduce its penetration in  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> support and therefore a smooth and homogenous mesoporous BTESO layer can be fabricated. The use of viscosity modifiers in the BTESO dip-sol can also be an option to form stable and uniform BTESO layer on  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> support.

**Chapter 7** compiles the overall conclusions drawn from the research with an outlook for future prospects. It was shown that apart from sol process parameters, pore tuning of hybrid silica membranes can also be accomplished by elemental doping or ageing of the freshly prepared membranes. Membranes fabrication, as described in chapter 3, can be utilized in biogas purification / upgrading. Successful hydrothermal and chemical stability tests of membranes presented in chapter 5 would lead to a new class of hybrid malonamide membranes that can withstand challenging industrial conditions without compromising on performances. Membrane pore orchestration can also be performed with strategies such as monomer templating, where small monomers can be incorporated in the BTESE matrix during synthesis followed by their removal during thermal treatments.

# Samenvatting

In dit proefschrift worden de bereiding en eigenschappen beschreven van verschillende hybride silica membranen, gebaseerd op organisch gebrugde siloxaan verbindingen. De beschreven membranen kunnen toegepast worden in verschillende moleculaire scheidingsprocessen. Aandacht wordt besteed aan verschillende procesparameters, die een belangrijke rol spelen bij het vormen van de poriestructuur in deze microporeuze membranen.

In **hoofdstuk 1** wordt een overzicht gegeven van de fabricage van silica membranen uitgaande van een zuur gekatalyseerde solbereiding. Deze membranen vertonen een bijzonder hoge selectiviteit onder droge omstandigheden. Echter, in een vochtige, hydrothermale, omgeving neemt de selectiviteit snel af vanwege de inherente instabiliteit van deze silica systemen in stoom. Om deze instabiliteit tegen te gaan worden in de literatuur twee strategieën vermeld: (1) toevoegen van metaalionen aan de silica matrix of (2) door de toevoeging van koolwaterstoffen in de silica matrix als brug tussen de silicium atomen of als eindgroep. Beide manieren van aanpak resulteerden in een verbeterde hydrothermale stabiliteit. In dit proefschrift zal met name aandacht besteed worden aan de mogelijkheid om koolwaterstof gebrugde silica membranen te kunnen gebruiken voor gasscheiding.

In **hoofdstuk 2** wordt een reproduceerbare bereidingsmethode beschreven voor een eenstaps sol synthese, uitgaande van een ethoxy-gebrugde silaan (1,2-bis(triethoxysilyl)ethaan: BTESE). Uitgaande van deze sol is, door middel van één enkele dip en calcineer stap een membraan verkregen met een meer open poriestructuur dan pure silica membranen. De synthese parameters in de solbereiding, zoals concentratie van de uitgangsverbinding (precursor), de zuurverhouding en de water/precursor verhouding, zijn zodanig geoptimaliseerd, dat een uniforme sol deeltjesgrootte is verkregen waarmee een defect-vrij membraan gemaakt kan worden, dat een goede H<sub>2</sub> permselectiviteit t.o.v. CO<sub>2</sub>, N<sub>2</sub> en CH<sub>4</sub> vertoont, terwijl deze membranen geen SF<sub>6</sub>-permeatie vertonen. Door de concentratie van de dipsol te variëren tussen 0.15 M en 0.6 M werden membraanlagen verkregen variërend van 90 tot 500 nm in dikte.

Met de kennis, verkregen uit het onderzoek zoals omschreven in hoofdstuk 2, is in **hoofdstuk 3** een methode beschreven voor de fabricage van een hybride silica (BTESE) membraan met verbeterde permselectiviteit. De bereiding van een BTESE sol gaat veel sneller (in 30 in plaats van 90 minuten) in vergelijking met de methode

zoals beschreven in hoofdstuk 2, door de zuur concentratie tijdens de sol synthese met een factor 15 te verlagen. Deze aangepaste synthesesmethode geeft membranen met een kleinere poriegrootte en resulteert in membranen die voldoende waterstof en vrijwel geen stikstof of methaan doorlaten bij 200 °C ( $H_2/N_2$  en  $H_2/CH_4$  permselectiviteiten van respectievelijk meer dan 50 en 90). Een defectvrije membraan microstructuur met een dikte van 400 nm kan worden verkregen door uit te gaan van een dip-sol concentratie van 0.6 M.

**Hoofdstuk 4** rapporteert het effect van het doteren van verschillend elementen in het BTESE op de membraan eigenschappen. Nieuwe sol-gel methodes zijn ontwikkeld voor het doteren van boor, niobium of tantaal in het BTESE. Microporeuze membranen zijn hieruit gemaakt door middel van een eenstaps dipproces. TGA-studies aan gedroogde gels en FT-IR-analyses aan gecalcineerde gels tonen aan dat er ethyleenbruggen zijn tussen de siliciumatomen in de metaal gedoteerde BTESE materialen en dat deze systemen thermisch stabiel blijven tot een temperatuur van tenminste 500 °C in een inerte gas atmosfeer. Gaspermeatie experimenten tonen aan dat deze gedoteerde BTESE systemen een meer open porie structuur hebben dan de ongedoteerde BTESE membranen. Aan de hand van hoge resolutie SEM-opnames is aangetoond dat geen (micro)scheurtjes in het membraanoppervlak aanwezig zijn.

Om een nog betere verdeling van metaalionen in een hybride silica matrix te verkrijgen is een nieuw type hybride-silica precursor ontwikkeld, namelijk N,N,N',N'-tetrakis-(3-ethoxysilyl)-propyl)-malonamide (TTPMA) en beschreven in **hoofdstuk 5**. TTPMA werd gesynthetiseerd onder base-gekatalyseeerde condities en cerium of nikkel ionen werden gebonden aan het malonamide ligand. TEM-analyse van gecalcineerde ( $T = 250$  °C) Ce-TTPMA en Ni-TTPMA gels toonden respectievelijk ceriumoxide nanodeeltjes (2-4 nm) en nikkeloxide nanodeeltjes (2-15 nm) aan. HR-SEM opnames van gecalcineerde membraanoppervlakken toonden aan dat beide type membranen defectvrij waren. De Ce-TTPMA membranen hadden een laagdikte van slechts 35 nm en een iets betere  $H_2/N_2$  en  $H_2/CH_4$  permselectiviteit bij 200 °C dan BTESE membranen. Ni-TTPMA membranen vormden een selectieve laag met een dikte van ongeveer 210 nm en hadden een gaspermeatie die een orde grotere lager was voor de kleine gas moleculen (d.w.z. He,  $H_2$ ) in vergelijking met BTESE

membranen, terwijl er geen aantoonbare permeatie van  $N_2$  of  $CH_4$  werd gevonden. Dit geeft aan dat Ni-TTPMA een dichter porienetwerk heeft dan BTESE membranen.

**Hoofdstuk 6** geeft de synthese en karakterisering weer van het hybride silica materiaal 1,2-bis(triethoxysilyl) octaan (BTESO) als een mogelijk alternatief voor de mesoporeuze  $\gamma-Al_2O_3$  membraantussenlagen.  $\gamma-Al_2O_3$  membranen hebben een beperkte stabiliteit onder extreme pH en hydrothermale omstandigheden. Vervanging van  $\gamma-Al_2O_3$  door BTESO zou het mogelijk moeten maken om membranen toe te kunnen passen onder omstandigheden waar chemische en hydrothermale stabiliteit van groot belang zijn. BTESO solen met een gemiddelde deeltjesgrootte van 25 nm werden gemaakt d.m.v. een zuur gekatalyzeerde sol synthese. Gecalcineerde BTESO gels lieten een mesoporeuze structuur zien. Echter, de BTESO sol infiltreerde in het  $\alpha-Al_2O_3$  drager materiaal tijdens de dipcoating procedure zonder dat er een laag op de drager werd gevormd. Dit werd waarschijnlijk veroorzaakt door de relatief kleine deeltjesgrootte van de BTESO sol in vergelijking met de poriegrootte van de  $\alpha-Al_2O_3$  drager (80 nm). Om een BTESO laag op een dergelijke drager aan te kunnen brengen is waarschijnlijk een gemiddelde sol deeltjesgrootte noodzakelijk van ten minste 40 nm. Het gebruik van viscositeitsregulatoren in de BTESO dip-sol kan ook een optie zijn om een stabiele en uniforme BTESO laag op de  $\alpha-Al_2O_3$  drager te vormen.

**Hoofdstuk 7** tenslotte geeft een overzicht van de belangrijkste conclusies en geeft aanbevelingen voor verder onderzoek. Er is aangetoond, dat naast het aanpassen van de sol bereidingsparameters, de poriegrootte van hybride BTESE silica membranen ook aangepast kan worden door andere elementen aan het BTESE toe te voegen of het membraan te “verouderen” voordat het gecalcineerd wordt. De membranen, zoals beschreven in hoofdstuk 3, kunnen bijvoorbeeld toegepast worden in het zuiveren/verbeteren van biogas. Als ook aangetoond kan worden dat de van TTPMA afgeleide membranen een goede hydrothermale en chemische stabiliteit vertonen, dan kan deze nieuwe klasse van membranen een interessant alternatief zijn. Het arrangeren van de poriegrootte van de deze membranen kan ook uitgevoerd met strategieën zoals monomeer “templating”, waar kleine monomeren in de BTESE matrix worden opgenomen tijdens de synthese gevolgd door het verwijderen van de template door thermische behandelingen.

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